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Entry Transition Water Surface Profile Prediction in Supercritical Partially Filled Pipe Flow



Dr. J. A. Swaffield

Service Systems Program Center for Building Technology U.S. Department of Commerce National Bureau of Standards Washington, DC 20234

and

Drainage Research Group Department of Building Technology **Brunnel University** U.K.

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U.S. DEPARTMENT OF COMMERCE, Malcolm Baldrige, Secretary NATIONAL BUREAU OF STANDARDS, Ernest Ambler, Director



PREFACE

This report is one of a group documenting National Bureau of Standards (NBS) research and analysis efforts in developing water conservation test methods, models for technical and economic analysis, and strategies for implementation and acceptance of practices. This work is sponsored by the Department of Housing and Urban Development, Office of Policy Development and Research, Building Technology and Standards Division, under HUD Interagency Agreement H-48-78.

SUMMARY

The criteria governing the development of steady partially filled supercritical pipe flow are presented together with the necessary techniques to determine the water surface profile in the pipe entry transition length.

The establishment of full bore flow is predicted for a range of flow rates and pipe design parameters. Based on the water surface profile calculation technique pipe length predictions are presented to avoid the air pressure fluctuations in the drainage system that result from full bore flow establishment.

Tabular data are presented to allow design decisions to be made that link pipe slope, diameter and roughness to the need to avoid full bore flow. A graphical technique is also presented that removes the necessity to interpolate from the tabular data.

The effect of entry geometry loss coefficients is included in the techniques presented.

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NOTATION

A ·	Channel cross sectional area					
С	Chezy constant					
D	Pipe diameter					
E	Specific energy					
g	Acceleration due to gravity					
h	Flow depth					
h _c	Critical flow depth					
h _e	Entry flow depth					
h _n	Normal flow depth					
L	Transition length					
m	Hydraulic mean depth					
n	Manning coefficient					
P	Wetted perimeter					
Q	Flow rate					
S	Slope of energy grade line					
So	Channel slope					
T	Water surface width in channel					
V	Local average velocity					
x	Axial flow direction					
Z	Elevation channel above some datum					
ρ	Fluid density					
θ_1	Approach pipe slope					

Test pipe slope

 θ_2



1. INTRODUCTION

In the design of building drainage systems the maintenance of appliance trap seals is a major criterion. Trap seal depletion may occur as a result of either negative or positive air pressure transients in the drainage pipework. Positive pressures may be generated if the water flow in the system becomes full bore at some downstream location. The most common cause of such a closure of the air passage above the water surface is the flow depth change that accompanies a change in pipe slope. The transition from vertical stack flow to the near horizontal building drain, commonly set at gradients in the range 1/40 to 1/80, results in a rapid depth increase downstream of the slope change that may result in the establishment of local full bore flow. Transition from the entry depth to a greater depth can be erroneously interpreted in experimental observations as an hydraulic jump; the theoretical predictions developed here indicate that a monotonically increasing (smooth) depth change can occur. The conditions under which a hydraulic jump exist are discussed in an earlier study [1].

The design criteria necessary to avoid this condition are set out in this report, together with the necessary computing techniques and design table examples for a range of typical pipe diameters, gradients and flow rates.

2. THEORETICAL CONSIDERATIONS

2.1 STEADY, UNIFORM FLOW IN PARTIALLY FILLED PIPE FLOW

Figure 1 illustrates the force balance equation for steady flow in an open channel or partially filled duct. The common expression of this relationship is known as the Chezy equation where

$$V = C \sqrt{m S_0}$$
 (1)

m = hydraulic mean depth A/P, m

 $S_0 = \sin \theta$, duct slope V = mean velocity, m/s

C = Chezy constant.

The value of loss coefficient C was found by Manning to be dependent on hydraulic mean depth and duct surface roughness n. The Manning formula is the simplest of the open channel equations:

$$V = \frac{1}{n} m^{2/3} S_0^{1/2}$$

$$Q = \frac{1}{n} A m^{2/3} S_0^{1/2}$$
(2)

where Q is the flow rate m^3/s A is the flow cross sectional area, m^2

The value of the Manning coefficient, n, varies with pipe or channel material. Chow [2] suggests values in the range 0.009 to 0.020 for materials commonly found in building drainage systems. The utilization of n as a variable with depth can be introduced (in the computer program) for more detailed calculations. The effects of wall accumulations on n as a function of deposited materials is unknown.

Equation 1 effectively determines the flow depth, h, under steady, uniform conditions, only one value of h yielding the values of A and m necessary to satisfy the equation. As this depth is by definition constant downstream, dh/dx=0, it must also be the terminal depth corresponding to the flow terminal velocity at that channel slope.

This depth, hn, is commonly referred to as the normal depth.

The specific energy of the flow may be defined as

$$E = h + \frac{v^2}{2g} \tag{3}$$

where h = local flow depth, m

V = local average flow velocity, m/s

Figure 2 illustrates the alternate depths that will satisfy equation (3) and their significance in terms of the flow definition.

From equation (3) and figure 2 it may also be seen that the flow specific energy has a minimum value below which the given flow conditions cannot exist. In a general, non rectangular channel this value may be determined:

$$E = h + Q^{2}$$

$$\frac{dE}{dh} = 0 = 1 - \frac{Q^{2}}{gA^{3}} \frac{dA}{dh}$$
(4)

From figure 3

$$dA = T dh (5)$$

where T is the surface width at any depth, h.

From equations (4) and (5) the minimum value of E will occur at a depth value, h_c , that satisfies the expression

$$1 - Q^2 T / g A^3 = 0 ag{6}$$

This value of h is referred to as the flow critical depth hc.

If the normal flow depth h_n exceeds h_c then the terminal flow would be termed subcritical, or tranquil flow. If h_n is less than h_c then the flow is termed rapid or supercritical.

It should be stressed that $h_{\rm C}$ is independent of pipe slope and pipe surface roughness; while the normal depth is dependent on both. Thus the same volume flow rate in any particular pipe may be rapid or tranquil depending on pipe slope, and similarly the same flow rate in a series of constant diameter pipes will be tranquil or rapid depending on roughness.

Pipes or channels in which rapid flow is normal are termed steep, pipes or channels in which tranquil flow is normal are termed of mild slope.

2.2 ENTRY TRANSITION LENGTH IN PARTIALLY FILLED PIPE FLOW

It will be seen from figure 2 that the flow depth at any point along a partially filled drain is dependent on both flow rate and specific energy. However the only stable depth is that represented by the normal flow equation, (2), thus a transition region may be expected in any partially filled pipe flow when the inlet flow conditions, expressed in terms of Q and E, do not match the normal depth characteristic values.

At the base of a vertical stack it is unlikely that the flow rate and specific energy will match the downstream drain normal depth values. In general the specific energy at the drain inlet will be higher than the normal depth and

flow characteristic specific energy, so that the entry flow depth will be less than the downstream normal depth.

Under these conditions frictional forces acting on the fluid flow result in an increase in flow depth downstream until the flow normal depth is reached. Thus a transition regime may be identified whose length is dependent on the pipe slope, diameter and roughness and the entry flow rate and specific energy. Figure 3 illustrates this transition region. This description is generally true whether the flow downstream is classified as subcritical or supercritical.

For the subcritical flow case, the normal depth to be achieved is greater than the flow critical depth and hence its establishment requires the generation of a hydraulic jump. This topic was dealt with in an earlier report [1].

For the supercritical flow case the depth profile may increase downstream until the normal depth is achieved without the generation of a hydraulic jump, or local flow depth discontinuity.

It is however necessary to distinguish clearly between the generation of local full bore flow due to a hydraulic jump and the observation of full bore flow as a result of a "smooth" transition to normal depth in supercritical flow. Comparison of the normal depth, calculated from equation (2), to the critical depth, as calculated from equation (6), is sufficient to determine whether a jump will occur, or whether it is sufficient to only consider the developing supercritical flow depth profile.

Care should be taken in any literature survey of drainage studies in this area as the term "hydraulic jump" is often used loosely to identify both the true jump condition and the establishment of full bore flow as a result of the supercritical depth transition described above.

In both cases the likelihood of full bore flow is predictable from a comparison of the target normal depth with the pipe diameter.

In the analysis presented steady flow conditions are assumed at a range of flow rates. In practice the entry flow to the drain will follow some flow vs time profile. Thus the establishment of full bore flow will depend on the peak entry flow rate and its attenuation as the inflow surge progresses down the pipe. A study of attenuation in supercritical free surface flow [2] indicates that the effect will be small over the first 5 to 6 m of drain so that it is reasonable to base design tables on the assumption that the entry profile may be represented by a series of increasing steady flow rates. Adjustments for the flow increase to permit adjustment for the series of stepwise increased rates may be made in the integrands of the equations in this report.

In order to provide design data two calculation techniques are required:

(1) Comparison of flow normal depth with both the drain critical depth value to determine the applicable flow regime, and the pipe diameter, to determine whether full bore flow is possible at this combination of flow rate, pipe diameter, gradient and roughness.

(2) Calculation of the water surface profile from the pipe entry downstream to either the establishment of normal depth flow or full bore flow. The necessary equations for (1) above have been established. The calculation of the water surface profile requires the use of gradually varied flow analysis.

2.3 GRADUALLY VARIED FLOW IN PARTIALLY FILLED PIPES

Gradually varied flow is steady non-uniform flow of a special type. The flow parameters are assumed to change slowly, if at all, in the flow direction. The basic assumption in the treatment of this type of flow is that the local head loss at any section is given by the Manning expression, (2), for the identical local flow depth and rate under assumed steady, uniform flow conditions.

Depth profile predictions by numerical integration are based on this assumption, expressed in terms of figure 4 by

$$\frac{d}{dL} \left\{ \frac{V^2}{2g} + (Z_0 - S_0 L) + h \right\} = -\left\{ \frac{nQ}{Am^2/3} \right\}^2$$
 (7)

where $(Z_O - S_O L)$ is the elevation at distance L along the channel, measured in the downstream direction; S_O is sin Θ , channel bed slope,

hence
$$-\frac{V}{g}\frac{dV}{dL} + s_0 - \frac{dh}{dL} = {nQ \choose \Delta_m 2/3}^2$$
 (8)

and as, Q = VA

$$\frac{dV}{dL} A + V \frac{dA}{dL} = 0$$

and as dA = T from equation 5 it follows that

$$\frac{dV}{dL} = \frac{V}{A} \frac{dA}{dL} = -\frac{VT}{A} \frac{dh}{dL} = -\frac{QT}{A^2} \frac{dh}{dL}$$

and substituting in equation (8) yields

$$Q^{2}T dh + S_{0} - dh = \left\{ \begin{array}{c} n Q \\ A m^{2}/3 \end{array} \right\}^{2}$$

$$dL = \left\{ \begin{array}{c} 1 - Q^{2}T/g A^{3} \\ S_{0} - (nQ/Am^{2}/3) \end{array} \right\} dh$$
(9)

or

$$L = \int_{0}^{h_{1}} 1 - Q^{2}T/gA^{3} dh$$

$$h_{0} S_{0} - (nQ/Am^{2}/3)^{2}$$
(10)

where L is the distance between two known depths ho, hl.

Figure 5 illustrates this numerical integration, which may be conveniently achieved by Simpson's rule.

The numerator and denominator of equation (10) will be recognized as the equations determining the critical and normal flow depths in an open channel.

When the term $(1 - Q^2T/gA^3)$ is zero the flow is at critical depth, i.e., there is no change in L for a change in h.

For uniform cross section channels with constant roughness, n, and slope, S_0 , the expression (10) becomes solely a function of flow depth h.

In order to numerically evaluate (10) it is necessary to define boundary conditions from which the integration may proceed. It should be stressed that the integration may be carried out either upstream or downstream from a known depth point. This ability is central to the use of this technique to determine the position of a profile continuity, such as a hydraulic jump.

Figure 5 illustrates the control depths used in the prediction of the water surface profiles in the case being investigated, namely the change in slope of an open channel.

If the flow rate Q and specific energy are known at pipe entry, at B, figure 3 then the depth at B may be calculated by choosing the lower depth root of equation (4). In the study reported a range of entry specific energy values for a constant inflow were obtained by considering the entry flow at B to have attained terminal flow conditions in an approach pipe, AB figure 3, set at a range of gradients from 15° to 90°, however this artifice is not strictly necessary as any suitable energy values could have been utilized.

The choice of dh values in the numerical integration is based on the difference between the control depth at entry and the "target" depth, representing the normal flow depth to be achieved downstream.

For the example in figure 5 the dh value is

$$dh = (h_n - h_e)/N$$
 (11)

where N is a reasonable number in the range 10--30. Since the change from h_e to h_n can be expected to fall within an order of magnitude and the monotonic change (except for the jump condition) in the function h(L) is not rapid the size of incremental steps can be of the order of unity.

If the normal depth, h_{n} , exceeds the pipe diameter, D, then the numerical integration is terminated when the predicted flow depth exceeds the pipe diameter value.

2.4 LOSS COEFFICIENTS FOR SLOPE TRANSITIONS IN PARTIALLY FILLED PIPE FLOW

No data could be obtained on the loss coefficients for slope transitions in open channel flow. For this reason the results presented assume no loss at the pipe entry. The computer program as written has been designed to include such a loss coefficient, in the range 0 to 1, should such data become available from a future experimental program. The effect of such a loss would be to increase the flow depth at pipe entry, with a consequent decrease in the kinetic energy term at pipe entry. In turn this would have the effect of generally moving the energy transition upstream towards pipe entry. Experimental work is required as a back up to the computer simulation to clarify this area.

3. CALCULATION TECHNIQUES AND PRESENTATION OF RESULTS

3.1 DETERMINATION OF NORMAL AND CRITICAL DEPTHS

The bisection method was used to solve the equation defining both critical flow depth

$$x = 1 - Q^2T/gA^3$$

and normal flow depth

$$Y = S_0 - (n Q/Am^2/3)^2$$
.

It may be assumed that both X and Y have zero values for some value of depth h in the range $0 \le h \le D$ for pipe case or $0 \le h \le W$ for the square section case.

This initial interval is bisected and h = D/2 or w/2 for the square section) used to evaluate X, Y. If the resulting values are positive then the root is less than the midpoint. The upper limit is then reset equal to the h value just used and the remaining interval bisected. The process repeats until a root is obtained. If the X or Y value had been negative then the root would be greater than the trial h value. In this case the lower limit is reset to the trial h value and incremented with the remaining interval bisected.

Due to the need to include the area depth relationship this solution must be undertaken by an iterative process. The computer time taken depends on the complexity of the area-depth function.

3.2 NUMERICAL INTEGRATION FOR SURFACE PROFILES

The integration of the position vs depth profile

$$L = \int_{h_0}^{h_1} \frac{1 - Q^2 T / g A^3}{s_0 - (nQ / Am^2 / 3)^2} dh$$

is achieved by means of Simpson's Rule. Let the integral $X = \int_{h_0}^{h_1} F(h) dh$,

then if the interval $\mathrm{h}_1\text{--}\mathrm{h}_0$ is divided into 2 equal increments, the value of X is given by

$$X = \frac{1}{3} dh [F(h_0) + 4F(h_0 + dh) + F(h_0 + 2 dh)]$$

As the integration moves on the length traversed may be accumulated as L = L + X at the completion of each integration.

3.3 PRESENTATION OF RESULTS

The transition profiles for the following cases are presented in tabular form in Appendix I:

Flow rates 2 to 12 ℓ /s, extended to 22 ℓ /s for the 0.15 m diameter pipe case

Pipe diameters: 0.075 m, 0.10 m and 0.15 m

Roughness coefficients: 0.009, 0.012, 0.015, 0.018

Pipe gradients: 1/20, 1/40, 1/60, 1/80

Entry specific energy range simulated by varying the approach pipe slope from 15° to 90°.

In addition to tabular data, an alternative graphical technique is presented.

3.4 INPUT DATA CHOICE

As far as possible the choice of input test conditions was governed by the range of values likely to be found in drainage systems. The pipe diameters chosen, 0.075, 0.10 and 0.15 conform to this criterion as do the pipe gradients used for all test cases, 1/40 to 1/80. The choice of pipe roughness or Manning coefficient was more difficult, however values in the range 0.009 to 0.015 are recommended in many texts, i.e. Jaeger [3] and Chow [4].

Losses at the change of slope that produces the conditions conducive to full bore flow have been ignored in this treatment. No available data on open channel transition loss coefficients for partially filled pipes or channels could be obtained. The program is capable of dealing with transition losses however via an input data control variable provided the loss can be expressed as a factor, 0 to 1.0, of the specific energy of the flow at pipe entry.

4. DISCUSSION OF RESULTS

The water surface profile integration downstream from pipe entry is illustrated by figures 6 and 7. It will be seen that the transition length, or the distance to full bore flow or normal depth, whichever is less, depends on both the flow rate and entry specific energy and hence any simplified prediction technique would have to include both these parameters.

The determination of whether or not full bore flow will occur at any particular combination of flow, Q, roughness, n, and pipe slope, S_{Q} , is rather simpler, depending on a comparison of normal depth to pipe diameter.

Figure 8 presents the normal depth to pipe diameter ratio as a function of a term $nQ/S_0^{1/2}$ that may be seen to determine normal depth from the Manning expression, equation (2). It will be seen that the curves for each of the three pipe diameters tend to become linear at the higher values of h_n/D . Thus a general equation may be proposed to indicate whether full bore flow is achievable, from figure 8,

$$h_{\rm n} = 0.14 + 0.0018 \, {\rm p}^{-2.67} \cdot {\rm nQ} {\rm S}_{\rm o}^{1/2}$$
 (12)

Once the establishment of full bore flow has been predicted it becomes necessary to determine whether this will occur within the system pipe length. The tables presented in Appendix I allow this calculation provided that the inflow rate and specific energy are known together with pipe slope, roughness and diameter.

Obviously if the transition length predicted is less than the required pipe length then design alternatives would include an increase in pipe slope, an increase in pipe diameter or the use of a smoother pipe, although it is recognized that this last alternative is unlikely to be employed.

The use of such tabular data is considered practical, however a graphical technique would have advantages in terms of the appreciation of effect of rapid design changes.

The problem to be solved here is the dependence of transition length on entry energy, however this may be bypassed if the entry depth is calculated.

Figure 9 presents the entry depth for any flow rate and specific energy combination for the three pipe diameters condensed in the form

$$h_e/D = f(Q, E)$$

$$(h_e/D)/Q = f_1(E)$$

Thus for any Q and E values the entry depth he may be read off figure 9.

It was found that the transition length at any pipe roughness, gradient, inflow rate and specific energy could be expressed in terms of

$$L/D = f(h_n/D - h_e/D)$$

as illustrated in figure 10.

For example, for a given flow rate the entry depth will decrease as the entry specific energy increases. Hence the depth change to be achieved to either full bore flow or normal depth increases as the entry energy rises. Therefore it would be reasonable to expect that the transition length would increase as the entry depth decreased, as shown in figure 10.

The curves in figure 10 apply to the specified one pipe diameter at one pipe slope at a range of pipe roughness coefficients. Obviously such curves may be generated from the data presented in appendix 1 for all the test cases.

It will be noted that individual points are plotted in figure 10 in the manner normal for test results and display a degree of scatter. This is due to the use of either pipe diameter or normal depth as the depth downstream target, whichever is the smaller value. This leads to a slight incompatibility between transition lengths to either D or h_n . However this scatter of the order of 2 to 3 percent and is well within the other uncertainties in the design of drainage systems, so that this technique may be proposed as a rapid visual method of determining the effect of design changes.

The tabular data presented in appendix 1 may be utilized if the entry flow rate and specific energy are known. Referring to table 1, reproduced from appendix 1, it will be seen that it will be necessary to employ an interpolation technique to determine the transition length if the flow entry rate and specific energy do not match the values given. The curves based on the tabular data presented above indicate that a simple linear interpolation would be sufficient. The format of the data, table 1, could be simplified as the approach pipe slope is, as mentioned, only included as a convenient method of determining a range in inflow specific energies.

Similarly the data could be rearranged in terms of constant inflow rate blocks instead of the constant approach pipe slope utilized in appendix l and table l.

The data presented has been based on inflow rate and specific energy and does not include an entry loss coefficient. In practice the form of the entry junction from, for example, a vertical stack to the building drain would lead to a junction loss coefficient that would appear, for any given flow rate, as a reduced specific energy.

Although this loss coefficient is not included in the presented data, it is automatically accounted for in the prediction method outlined above. A reduction in specific energy for any flow rate effectively increases the entry depth, figure 9, and hence reduces the transition length, figure 10, for any one set of pipe design parameters.

In the absence of published data on such loss coefficients, experimental work is suggested to fill this gap and the inclusion of an estimated loss coefficient is recommended in the application of the presented data.

5. CONCLUSIONS

In supercritical flow in a partially filled pipe a transition region may be identified at the pipe entry that allows the flow depth to increase to that compatible with the flow rate and pipe parameters (slope, roughness, diameter, etc.).

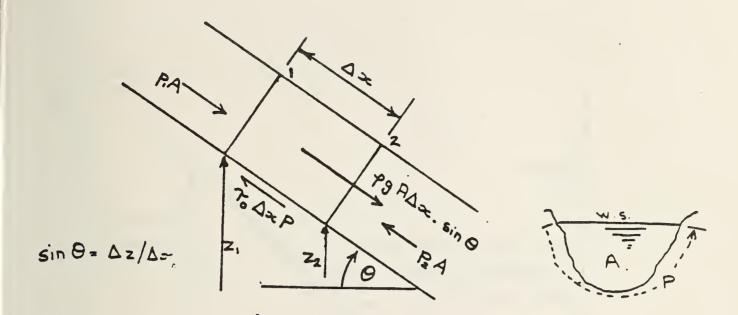
This transition may lead to the establishment of full bore flow if the pipe exceeds the necessary transition length at flow rates where the normal depth, as predicted by Mannings equation, exceeds the pipe diameter.

This study has identified the conditions necessary for full bore flow and has determined the transition lengths at a range of flow rates and pipe design parameters compatible with current drainage design.

It is stressed that the design data presented is based on entry flow and specific energy. Although no entry loss coefficient has been included, this effect is automatically accounted for in the design curves presented as an entry loss would merely reduce the flow specific energy at entry and would not affect the validity of predictions based on the data presented.

6. REFERENCES

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- Swaffield, J. A., Application of the Method of Characteristics to Predict Attenuation in Unsteady Partially Filled Pipe Flow, NBS Report, October 1980.
- 3. Jaeger, C., Engineering Fluid Mechanics, Blackie and Sons, London, 1956.
- 4. Chow, V. T., Open Channel Hydraulics, McGraw Hill, 1970.



From energy equation 1-2

Losses =
$$hf = P_1 - P_2 + Z_1 - Z_2$$
 fg

as $V_1 = V_2$; steady, uniform flow.

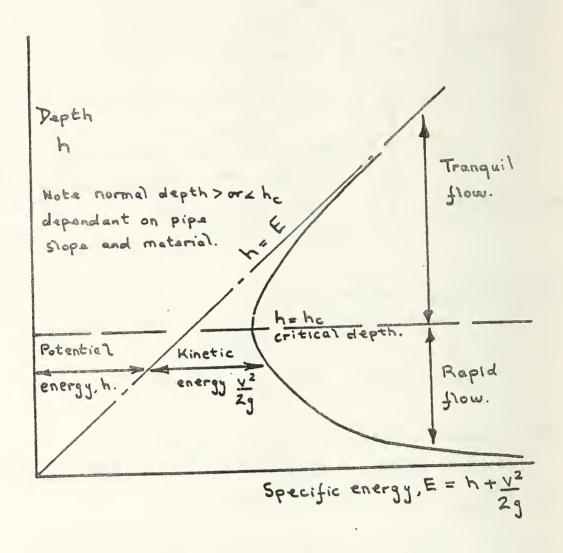
From momentum equation down slope $(p_1-p_2)A + p_3A\Delta x \sin \theta - T_0 \Delta xP = 0$ as dV/dt = 0; steady flow.

$$\frac{P_1 - P_2}{fg} + \Delta z = T_0 \frac{\Delta_{>c} P}{fg A} = h_f$$

For turbulant flow To = f = pv2

$$h_f = \int \frac{\Delta x e^{V^2}}{2gm}$$
, $V = C \int mS$, $S = \sin \Theta$
 $m = R | P$
 $C = constant$

Figure 1. Derivation of Chezy's equation for free surface flow



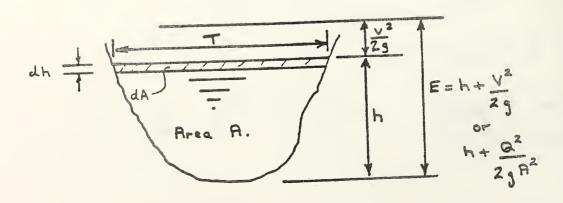
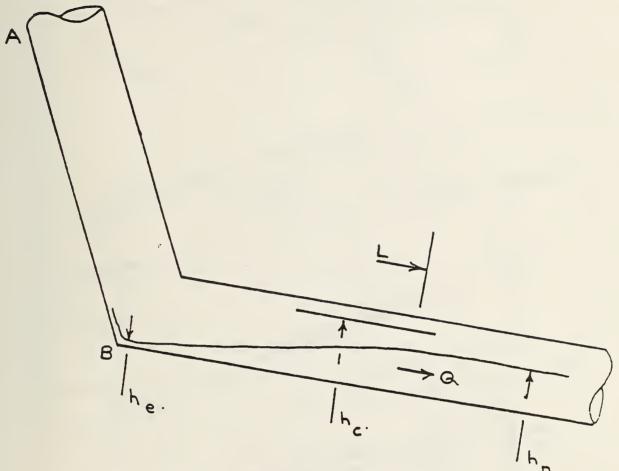


Figure 2. Relationship between flow specific energy and flow depth

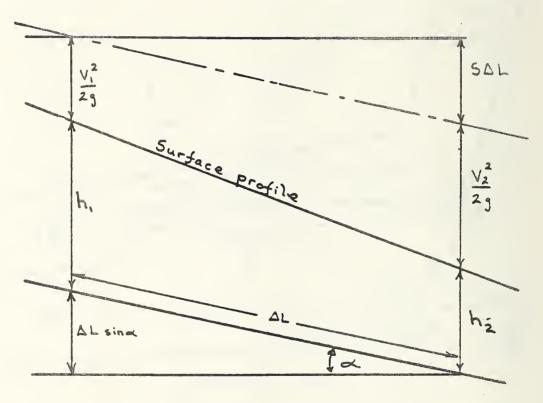


hn < hc, flow supercritical, no hydraulic jump forms.

he =
$$f(Q, E)$$
, $E = h_e + V_e^2/2g$
Transition length $L = f(h_e, h_n)$

Note transition length taken as L value for $h = 0.975 h_{R}$.

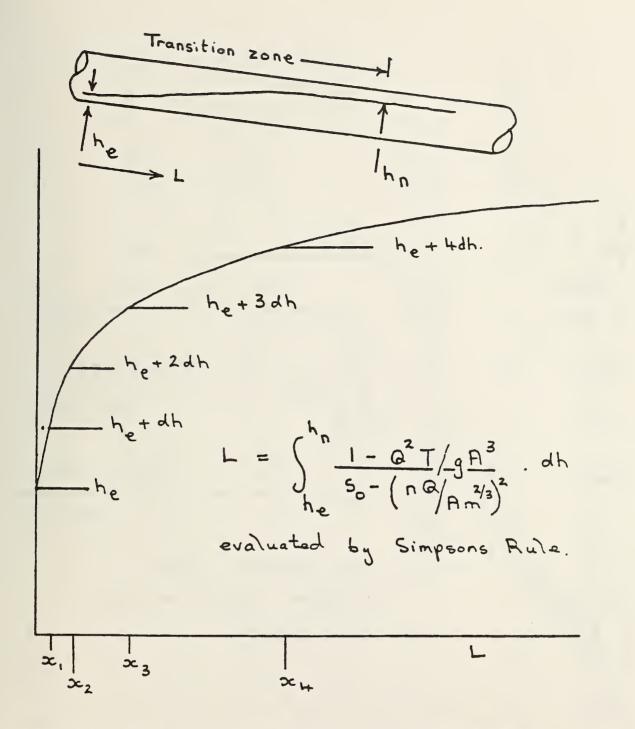
Figure 3. Transition length downstream of a pipe slope change in partially filled pipe flow



Gradually varied of low, analysis
based on head loss at any section
being equal to Manning loss
prediction, where

$$S = -\frac{\Delta E}{\Delta L} = \left(\frac{nQ}{A m^{2/3}}\right)^{2}$$

Figure 4. Basis of gradually varied flow analysis



Note (i) AL increases as L increases

(ii) water surface profile approaches normal depth as shown only in supercritical flow

Figure 5. Schematic representation of numerical integration to determine water surface profile

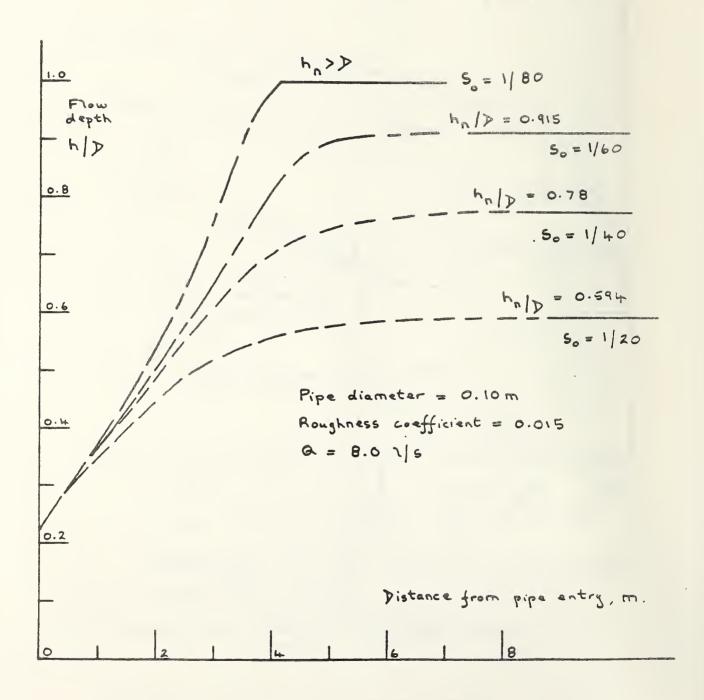
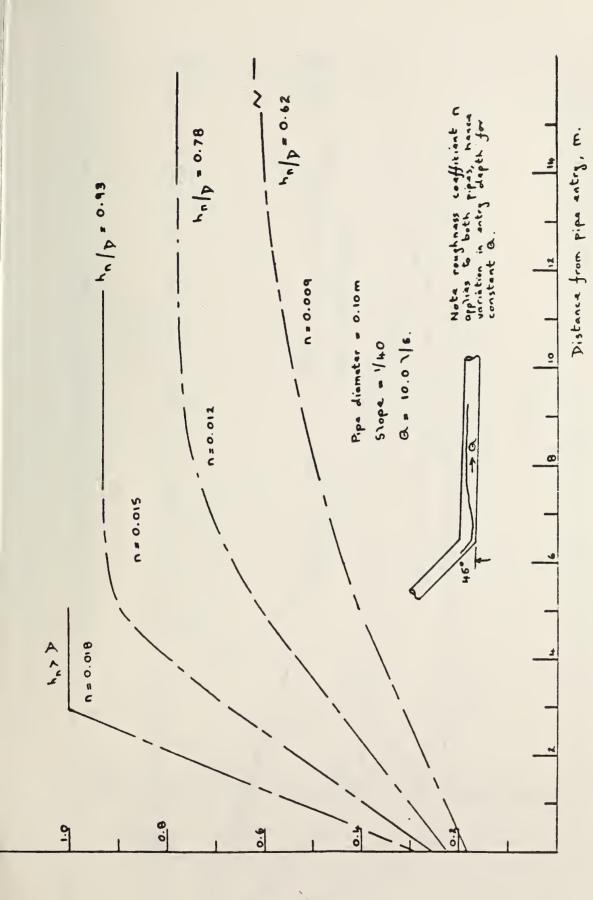


Figure 6. Water surface profiles for a range of pipe gradients, illustrating increase in transition length as pipe slope is increased



Water surface profile for a range of pipe roughness values, illustrating increased transition length as pipe roughness is decreased Figure 7.

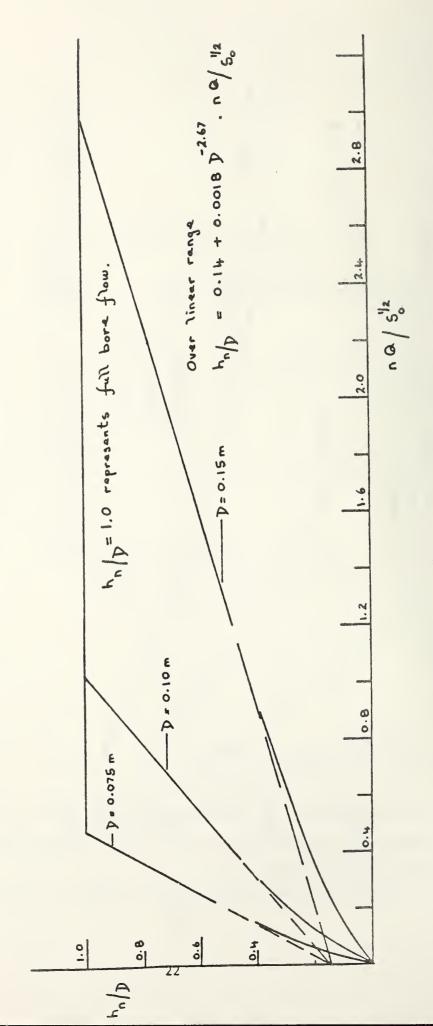


Figure 8. Flow normal depth as a function of pipe and flow parameters for a range of pipe diameters.

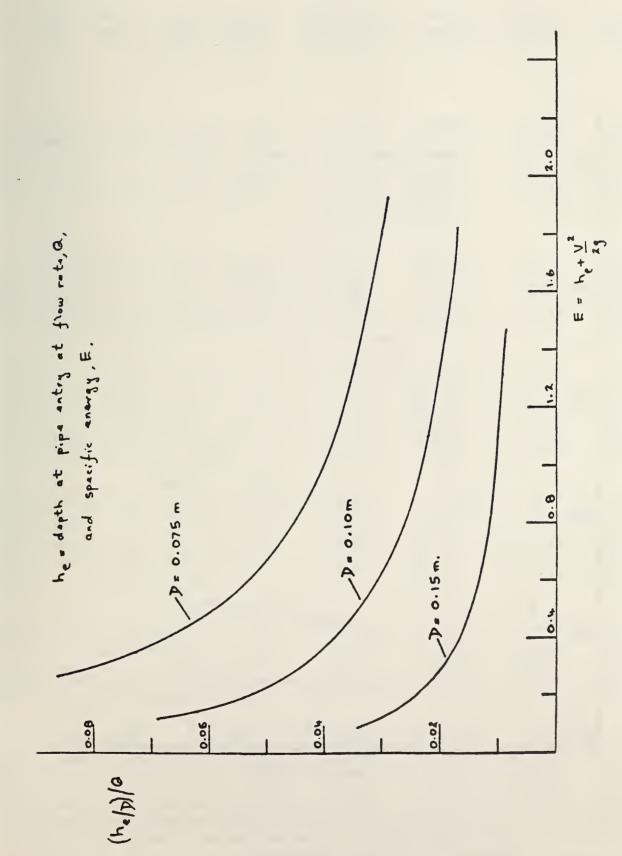


Figure 9. Entry depth as a function of flow rate and entry specific energy

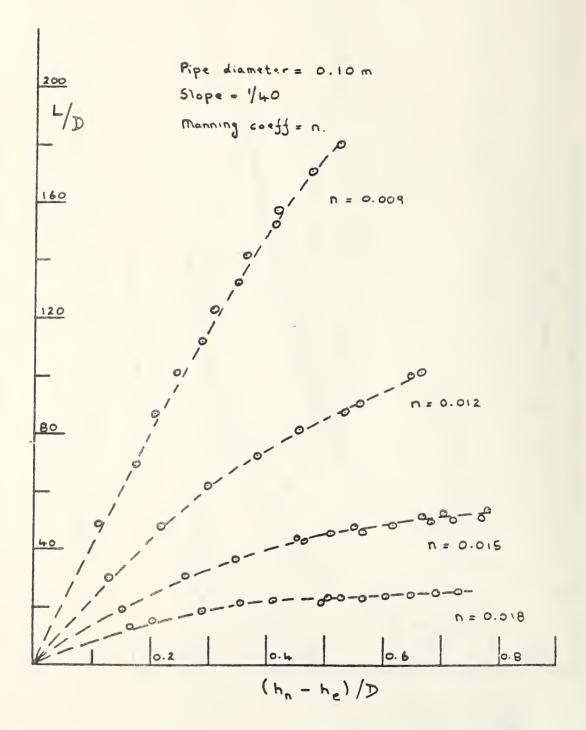


Figure 10. Transition length as a function of depth change from entry to normal depth, note that flow rate and entry energy are subsumed in the depth change term

И									
	FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLCPE	SLOPE	DRAIN FLOW ENTRY DEPTH	ENERGY	NORMAL DEPTH	PIPL LENGTH TO NORMAL JEPTH.
		•		(S1K) =	(SIN)	RATIO H/D	n.	H/D.	L/D.
			0.7390	-		0.1493	0.3003	0.2605	55.3110
			0.0090			0.2384	0.4714	0.4250	90.4655
			0.2090			0.3167	0.6021	0.5746	115.9573
			0.0010	_		0.3594	0.7091	0.7241	130.7753
			0.0010			0.4507	0.7999	0.8647	154.6711
	12.00	0.075	0.0040	0.2566	C.0500	0.5259	0.6782	1.0000	170.5312
	3 0 %	0 675	6 6000	0 4 0 6 6	0 (500	. 1204	0 4534	0.34.4	
			0.0030			0.1204	0.4534	0.2605	61.7167
			0.3030			0.1906	0.7241	0.4250	100.3700
			0.0740			0.2512	0.9377	0.5746	124.5554
			0.0000			0.3074	1-1143	0.7241	153.0397
			0.0000			0.3606	1.2059	0.5647	173.2925
	12.00	0.075	0.0340	3.5000	(• (. 2 - 3 0	0.4114	1.4015	1.0000	210.7971
	2 00	((76	0.2210	2 7676	C 01.00	L.1076	0.2646	Ŭ•26⊍5	64.2399
			0.2070			U-1576	0.9092	U. 4250	100.0142
			0. 7070						
						0.2230	1.1825	0.5746	120.07.5
			0.1070			0.2722	1.4117	0.7241	157.7544
			0.0090			0.31st	1.0105	0.8547	181.7117
	12.00	C. C 75	0.0010	0.7070	6.6500	0.363c	1.7572	1.0000	225.0757
	2 00	0.076	0.0010	0 8446	C (50.)	0.1358	0.0421	0.2605	65.5253
			0.0070			0.15oc	1.0369	0.42:0	107.1125
			C. 1020			U.2Jn1	1.3543	0.5796	137.4052
			0.1079			6.2537	1.0213	0.7241	163.2255
			0.3010			U.2966	1.0530	U. 0647	105.02/0
			0. 1710			0.2760	2.0654	1.0000	232.5050
		(• • • •)	C. 7.70	0.000	C • C 3 70	0.5572	2.00.	1.0000	232.3030
	2.00	0.075	0.0030	0.4659	0.0500	0.0974	0.6672	0.2505	66.1533
			0.0010				1.1131	0.42:0	10c.17-7
			0.2000			U. 200c	1.4567	J. 5740	134.3307
			0.2070			U.2444	1.7445	0.7241	104.7523
			0.0070			D. 2354	1.9990	0.8647	167.3756
			0.0040			0.3245	2.2277	1.0000	230.6107
							,		
					0.0500	· 0.0964	0.7010	0.2635	66.3314
	4.00	0.075	0.00+0	0.4462	(.0500	0.1512	1.1361	0.42 50	100.4943
			0.0010			0.1954	1.4:57	0.5740	134.7422
			0.0000			U.2416	1.7547	0.7241	165.4743
			0.0070			0.2320	2.0470	U. 5547	157.6113
	12.00	C.075	0.1010	0.941,2	6.6500	L.3210	2.2740	1 0000	23/.5351

Table 1. Typical Tabular Data for 0.10 m Diameter Pipe

APPENDIX 1

TABULAR DATA RELATING FLOW NORMAL DEPTH AND TRANSITION LENGTH TO FLOW AND PIPE PARAMETERS

Cases included:

 D = 0.075

FLOW L/S.	DIA.	MANY. COEFF	SUPPLY SLUPE (SIK)	CRAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RAIIO H/D.	ENTRY ENERGY n.	MORMAL DEPTH H/D.	PIPE LENGTH NORMAL JEPT L/U.
4.00 6.00 8.00 10.00	0.075 0.075 0.075 0.075	0.7990 0.7990 0.7990 0.7990 0.7990	0.25EE 0.25EE 0.25EE 0.25EE	0.0500 0.0500 0.0500 0.0500	0.1493 0.2384 0.3167 0.3394 0.4587	0.3003 0.4714 0.6021 0.7091 0.7499	0.2605 0.4230 0.5796 0.7241 0.8647	55.3110 90.4655 115.9573 130.7753 154.6711
2.00 4.00 6.00 8.00	0.675 0.675 0.675 0.675	0.0090 0.0090 0.0090 0.0090 0.0090	0.50C0 0.50C0 0.50C0	0.0500 0.0500 C.0500 C.0500	0.1204 0.1906 0.2512 0.3074	0.4534 0.7241 0.9377 1.1143	0.2605 0.420 0.5796 0.7241	61.7167 100.8709 129.5654 153.0399
2.00 4.00 6.00	0.075 0.075 0.075 0.075	0.0070 0.0070 0.0070 0.0070 0.0070	0.5000 0.7070 0.7070 0.7070	0.0500 0.0500 0.0500 0.0500	0.3606 0.4114 0.1076 0.1696 0.2230	1.2659 1.4015 0.5646 0.9092 1.1826	0.8647 1.0000 0.2605 0.4250 0.5746	173.2926 210.7071 64.2399 105.0192 135.0715
10.00	0.675	0.1070 0.0070 0.0070 0.0070	9.7C7C 0.7C7C	C.(500 0.6500 C.0500	0.31db 0.3630	1.4117 1.6103 1.7872 0.6421 1.0369	0.7241 0.8547 1.0000 0.2605 0.4210	159.7544 181.0117 225.0757 65.5258 107.1185
8.00 10.00 12.00	0.075 0.075 (.075	0.0090	0.8660 0.8660	0.0500 0.0500 0.0500	0.2001 0.2537 0.2966 0.3372	1.3543 1.6213 1.6530 2.0659	0.5746 0.7241 0.3647 1.0000	137.9052 163.2255 185.0276 232.3050
4.00 6.00 8.00 10.00	C. 075 G. 075 G. 075 O. 075	0.0090 0.0090 0.0090	0.9659 0.9659 0.9659	0.0500 0.0500 0.0500 0.0500	0.1530 0.2006 0.2444 0.2954 0.3245	1.1131 1.4567 1.7445 1.9990 2.2277	0.4250 0.5746 0.7241 0.8647 1.0000	106.1747 139.3347 164.9523 187.3756 236.6147
4.00 6.00 8.00 10.00	C.075 C.075 C.075 C.075	0.0090 0.0090 0.0090 0.0090 0.0090	0.9962	C.0500 C.0500 C.0500 C.0500	0.0964 0.1512 0.1904 0.2416 0.2320 0.3210	0.7010 1.1381 1.4687 1.7547 2.0470 2.2746	0.2605 0.4250 0.5746 0.7241 0.8647 1.0000	60.3314 100.4943 139.7435 165.4743 187.6373 237.5353

1	FLOH	DIA.	HANN.	SUPPLY	DRAIN SLOPE	DRAIN FLOW ENTRY DEPTH	ENTRY	NORMAL	PIPE LENGTH TO NORMAL DEPTH.
Н	C / 30		CO	(SIN)	(SIN)	RATIO H/D.	M.	H/0.	L/0.
П									
ı									
	2 00	A.076	0.0000	0.2588	06250	0.1493	0.3003	0.3328	74.7487
				0.2586		0.2384	0.4714	0.5542	116.5603
J.				0.2586		0.3167	0.6021	0.7593	147.3951
			-	0.2588		0-3844	0.7091	0.9556	160.7624
			-	0.2588		0.4567	0.7999	1.0000	105.4435
H	12.00	0.075	0.0070	0.2588	0.0250	10.5259	0.0782	1.0000	82.4533
R					•				
	2 22								
H				0.5000		0.1204	0.4534	0.3328	80.1538
ŧ.				0.5000		0.1906 0.2512	0.7241	0.5542 0.7573	125.5291
N				0.5000		0.3074	1.1143	0.7556	159.2294 163.1312
				0.5000		0.3606	1.2659	1.0000	120.8943
				0.5000		0.4114	1.4015	1.0000	101.9159
n									
						,			
				0.7070		0.1076	0.5646	0.3328	82.4540
ì				0.7076		0.1696	0.9092	0.5542	124.3949
				0.7070		0.2230	1.1625	0.75+3	164.3577
4				0.7070		0.2722	1.4117	0.9556	184.4252
				0.7070		0.3156	1.6108	1.0000	133.7221
	12.00	0.075	0.7070	0.7076	0.0250	0.3630	1.7872	1.0000	110.5250
1									
ñ	2.00	0.075	0.0090	0.8660	0.0250	0.1008	0.6421	0.3328	83.6575
0;				0.8660			1.0369	0.5542	131.4030
1				0.8660		0.2001	1.3543	0.7593	167.0721
ğ.				0.8666		0.2537	1.0213	0.9556	192.7649
				0.8666		0.2966	1.8530	1.0000	137.8971
	12.00	0.675	0.3093	0.8660	0.6250	0.3372	2,0659	1.0000	115.4011
	2.00	0.075	0.2040	0.9659	0.0250	0.0974	0.6872	0.3328	84.2522
ě.				0.9654		0.1530	1.1131	0.5542	132.4250
				0.9659		6.2006	1.4557	0.7593	160.4513
į.				0.9659		0.2444	1.7445	0.9556	194.475
				0.9659			1.9990	1.0000	140.0517
	12.00	0.075	0.0000	0.9659	0.0250	0.3245	2.2277	1.0000	117.7731
	2.00	0-075	0-0030	0.9962	r 1251	0.0964	0.7010	0.3328	84.4212
				0.9962			1.1381	0.5542	132.7350
				0.9964		0.1984	1.4887	0.75 + 3	160.8524
				0.9962			1.7047	0.9556	194.9522
	10.00	C.075	C. 33 10	0.9962	0.0250	0.2420	2.0470	1.0000	140.7102
	12.00	C.675	0.0010	0.4902	C.0250	0.3210	2.2746	1.0000	116.4150

FLOW L/S.	DIA.	MANN. CJEFF		GRAIN SLGPE (SIN)	DRAIN FLOW ENTRY DEPTH RAILO H/D.	ENTRY ENERGY	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPTH L/D.
4.00 6.00	0.075 0.075	0.0090 0.0090 0.0090 0.0090	0.2588 0.2588	0.0167	0.1493 0.2344 0.3167 0.3894	0.3003 0.4714 0.6021 0.7091	0.3850 0.6470 0.9921	84.0454 126.7449 155.3644 116.6959
10.00	0.075	0.0070	0.2568	0.0167	0.5394 0.4587 0.5259	0.7999	1.0000	73.6458
				0.0167		0.4534	0.3850	89.2367
6.00	0.075	0.0090	0.5000		0.1906 0.2512 0.3074	0.7241 0.7377 1.1143	0.6470 0.8921 1.0000	135.4462 167.4643 131.7243
		0.0070			0.3606 0.4114	1.4015	1.0000	100.7604
		0.0010			0.1076 0.1696	0.5646 0.4092	0.3850	91.49:1
6.00	0.075	0.0070 0.0070 0.0070	0.7C7C 0.7C7C	C.0167 0.0167	0.2230 0.2722	1.1826	0.8921 1.0000 1.0000	172.1701
		0.0090			0.3166 0.3630	1.6108	1.0000	101.2050
4.00	0.075	0.2090	0.8660	0.6167	0.1008 0.1536	0.6421	0.3850 0.6470	92.6928 147.0222
8.00 10.00	0.075	0.0090 0.0090 0.0090	0.866.	C.0167 C.0167	0.20dl 0.2537 0.2960	1.3543 1.6213 1.8530	0.8921 1.0000 1.0000	170.7551 141.4461 110.7650
12.00	0.075	0.1010	0.8660	C.0167	0.3372	2.0659	1.0000	105.9259
4.00	0.075	0.0090 0.0090 0.0090	0.9659	0.0167	0.0974 0.1530 0.2006	0.6672 1.1131 1.4567	0.3950 0.6470 0.8921	93.2647 155.7237 170.3251
10.06	0.075	0.0090 0.0090	0.9659	0.0167	0.2444 0.2854 0.3245	1.7445 1.9990 2.2277	1.0000 1.0000 1.0000	145.7405 120.3922 106.2743
		0.0070			0.0964	0.7010	0.3850	93.3151
6.00 8.00	0.075 C.075	0.0030	0.9962	C.Ulo7 C.Ulo7	0.1512 0.1954 0.2416	1.1381 1.4887 1.7647	0.6470 0.8921 1.0000	150.41v1 170.1441 144.2v33
		0.0030			0.3210	2.0470	1.0000	121.5425

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLCPE (SIN)		DRAIN FLOW ENTRY DEPTH- RATIO H/D.	ENTRY ENERGY	NURMAL DEPTH H/D.	PIPE LENGTH TO NORMAL DEPTH. L/O.
			***************************************	, , ,		•••	,	4,00
	•							
			0.2588		0.1493	0.3003	0-4280	87.0075
			0.2566		0.2334	0.4714	0.7241	128.2535
			0.2566		0.3167	0.5021	1.0000	165.2457
			0.2568			0.7041	1.0000	101.5207
			0.2568		U • 4537	0.7999	1.0000	83.6233
12.00	C.075	0.0000	0.2586	0.0125	0.5259	0.5782	1.0000	70.0330
							•	
2 00	0.075	0.0000	0.5000	0.0125	G-1204	0.4534	0.4280	93.0496
			0.5000		0.190t	0.7241	0.7241	130.9651
			0.5006			0.7271	1.0000	180.1003
			0.5(60			1-1143	1.0000	116.1131
			0.5000			1.2659	1.0000	100.37.39
			0.5000		0.4114	1.4015	1.0000	80.7007
12.00		0.0079	0.000		001221		1.0000	
		,					•	
2.00	0.075	0.0070	0.7070	0.0125	· 0.1076	0.5546	0.4280	95.2693
			0.7076		0.1696	0.4092	0.7241	144.5375
			0.7070		0.2230	1.1026	1.0000	180.7453
			0.7070		0.2742	1.4117	1.0000	122.6924
10:00	0.075	0.2020	0.7076	C. L125	0.3186	1.0108	1.0000	108.0052
12.00	0.075	0.0000	9.7070	0.6125	0.3630	1.7872	1.0000	97.2992
					•			
			0.8660		0-1008	0.6421	0.4260	94.1411
			0.8666		0.1536	1.6369	0.7241	149.5331
			0.8660		0.2031	1.3543	1.0000	190.25/3
			0.6660		0.2537	1.6213	1.0000	120.2343
			0.8660		0.2760	1.8530	1.0000	112.0943
12.00	0.075	0. 3035	0.8660	0.0125	0.3372	2.0659	1.0000	101.7938
						•		
2 - 00	(-(75	0-10-10	0.9659	0.0125	G-0974	0.6872	0.4260	93.5734
			0,5659		0.1530	1.1131	0.7241	152.3165
			0.9659		0.2006	1.4567	1.0000	192.0543
			0.9(59		0.2444	1.7445	1.0000	120.0131
			0 9659		0.2354	1.4990	1.0000	114.2175
			0.9659		0.3245	2.2277	1.0000	104.3309
					-			
			0.5962		0.0904	0.7010	0.4280	93.4051
			0.9962		0.1512	1.1381	0.7241	153.11.7
			0.9962		0.1954	1.4567	1.0000	192.5519
			0.9962		0.2410	1.7547	1.0000	120.5555
			0.4962		0.2820	2.0470	1.0000	114.2577
12.00	e.675	0.0000	0.9962	0.0125	0.3210	2.2745	1.0000	104.4037

FLOW L/S.	DIA.	COEFF	SLOPE SLOPE		ORAIN FLOW ENTRY DEPTH RATIO H/D.	ENERGY	NORHAL DEPTH	
					•		•	
								:
2.00	0-025	0.0120	A 2568	0.6500	0.1810	0.2102	0.3191	36.6319
		0.0120			0.2913	0.3257	0.5298	57.1439
		0.0120			0.3844	_	0.7241	
		0.0120			0.4812	0-4813	0.9116	
		0.0120			0.5698	0.5388	1.0000	
12.00	0.075	0.0120	0.2588	0.6500	10.6548	0.5901	1.0000.	37.2790
2.00	0.075	0.0120	0.5000	C.0500	0.1454	0.3157	0.3191	40.7864
		0.0120			0.2316	0.4980	0.5298	63.8034
		0.0120			0.3074	0.6369	0.7241	80.7601
		0.0120	-		0.3777	0.7511	0.9116	94.5010
		0.0120	- /		0.4446 0.5093	0.0483	1.0000	60.5540 50.2442
12.00	0.013	0.7120	0.5000	0.0000	0.3043	0.9320	1.0000	30.2442
		0.0120			0.1298	0.3924	0.3191	42.4726
		0.0120			0.2059	0.0232	0.5248	66.5518
		0.7120			0.2722	0.6030	0.7241	84.4010
		0.0120			0.3333	0.9533 · 1.0785	0.9116	90.9051 73.6009
		0.0120			0.4475	1.1918	1.0000	56.1702
						:		
2.00	0.075	0.0120	0.8666	0-0500	0-1214	0.4463	0.3191	43.3480
		0.0120				0.7117	0.5298	67.9977
		0.3120			0.2537	0.9203	0.7241	86.3142
		0.0120			0.3103	1.0940	0.9116	101.1972
		0.0120			0.3640	1.2430	1.0000	76.7545 59.3613
12.00	0.075	0.9120	0.6600	C. C. O. O. O.	0.4153	1.3/02	1.0000	24.3012
		0.0120			0.1172	0.4775	0.3191	43.7702
		0.0123			0.1852	0.7655		60.7412
		0.0120			0.2444	0.4693		87.27.2
		0.0120			0.2956 0.3479	1.1788	0.9116	102.3732
		0.7120			0.3497	1.4857	1.0000	60.9831
				3007,3				
		0.0120			0.1160	0.4873	0.3191	43.9010
		0.0120			0.1832	0.7014	0.5248	60.9401
		0.0120			0.2410 0.2952	1.2055	0.7241	37.5630 102.7105
		0.7120			0.2452	1.3719	1.0000	70.6630
		0.0120			0.3945	1.5180	1.0000	61.4203

2.00	0.01	FLOH L/S.	DIA.	MANY. COEFF	SUPPLY SLUPE (SIM)	DEAIN SLUPE (SIN)	HIARD YATHS	DEPTH	ENTRY ENERGY n.	NORMAL DEPTH H/D.	PIPE LENGTH TO MORMAL DEPTH. L/D.
4.00 C.C75 0.3120 0.2568 0.0250 0.3934 0.4116 0.956 80.0239 8.00 C.C75 0.7120 0.2586 C.C250 0.3394 0.4116 0.956 80.0239 8.00 C.C75 0.3120 0.2586 C.C250 0.4312 0.4013 1.0000 51.4024 10.00 0.675 0.3120 0.2586 0.0250 0.6598 0.3583 1.0000 33.6553 12.00 C.C75 0.3120 0.2586 0.0250 0.6548 0.3991 1.0000 29.5568 2.00 0.075 0.3120 0.5000 0.0250 0.2316 0.4980 0.9919 73.1474 4.00 C.C75 0.3120 0.5000 0.0250 0.2316 0.4980 0.9919 73.1474 6.00 C.C75 0.3120 0.5000 C.C250 0.3074 0.3089 0.9556 87.7921 8.00 C.C75 0.3120 0.5000 C.C250 0.3074 0.3089 0.9556 87.7921 10.00 C.C75 0.3120 0.5000 C.C250 0.3074 0.3089 0.9556 87.7921 12.00 C.C75 0.3120 0.5000 C.C250 0.30777 0.7511 1.0000 60.935 12.00 C.C75 0.3120 0.5000 C.C250 0.5033 0.4925 1.0000 40.5017 12.00 C.C75 0.3120 0.5000 C.C250 0.5033 0.4925 1.0000 40.5017 12.00 C.C75 0.3120 0.7670 C.C250 0.5033 0.4925 1.0000 41.5565 2.00 C.C75 0.3120 0.7670 C.C250 0.3296 0.3924 0.4099 50.7431 4.00 C.C75 0.3120 0.7670 C.C250 0.222 0.6033 0.4056 91.2774 8.00 C.C75 0.3120 0.7670 C.C250 0.3918 1.0000 6.4537 13.00 C.C75 0.3120 0.7670 C.C250 0.4475 1.1918 1.0000 6.4537 12.00 0.075 0.3120 0.7670 C.C250 0.4475 1.1918 1.0000 6.77477 12.00 0.075 0.3120 0.8660 C.C250 0.1214 0.4463 0.4099 51.5613 4.00 C.C75 0.3120 0.8660 C.C250 0.123 0.7117 0.4099 51.5613 4.00 C.C75 0.3120 0.8660 C.C250 0.123 0.7655 0.6919 77.3623 6.00 C.C75 0.3120 0.8660 C.C250 0.1244 0.4663 0.4099 51.9901 12.00 0.075 0.3120 0.9659 C.C250 0.1322 0.7655 0.6919 77.3641 12.00 0.075 0.3120 0.9659 C.C250 0.1322 0.7655 0.6919 77.3641 12.00 0.075 0.3120 0.9659 C.C250 0.1322 0.7655 0.6919 77.3641 12.00 0.075 0.3120 0.9659 C.C250 0.1322 0.7655 0.6919 77.3641 12.00 0.075 0.3120 0.9659 C.C250 0.1322 0.7655 0.6919 70.3641 12.00 0.075 0.3120 0.9659 C.C250 0.1320 0.4099 51.9901 12.00 0.075 0.3120 0.9659 C.C250 0.1320 0.4099 50.4099 50.4099 50.4099 50.4099 50.4099 50.4099 50.4099 50.4099 50.4099	The state of the s										
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4.00 0.075 0.0120 0.5000 0.0250		12.00	0.075	0.7120	0.2200	0.0250	0.65	70	0.5991	1.0000	29.5556
4.00 0.075 0.0120 0.5000 0.0250 0.3014 0.4980 0.0919 73.1474 6.00 0.075 0.0120 0.5000 0.0250 0.3074 0.0369 0.9556 87.7921 8.00 0.075 0.0120 0.5000 0.0250 0.3777 0.7511 1.0000 60.9355 10.00 0.075 0.0120 0.5000 0.0250 0.4446 0.3453 1.0000 49.5017 12.00 0.075 0.0120 0.5000 0.0250 0.5093 0.9325 1.0000 49.5017 12.00 0.075 0.0120 0.7670 0.0250 0.1296 0.3924 0.4079 50.7451 4.00 0.075 0.0120 0.7670 0.0250 0.2059 0.232 0.6919 75.7575 6.00 0.075 0.0120 0.7670 0.0250 0.2722 0.3033 0.9556 91.2748 8.00 0.075 0.0120 0.7670 0.0250 0.2722 0.3033 0.9556 91.2748 8.00 0.075 0.0120 0.7670 0.0250 0.3918 1.0000 59.4534 12.00 0.075 0.0120 0.7670 0.0250 0.3918 1.0000 59.4534 12.00 0.075 0.0120 0.7670 0.0250 0.4475 1.1918 1.0000 59.4534 12.00 0.075 0.0120 0.8660 0.0250 0.1923 0.7117 0.6919 77.1529 6.00 0.075 0.0120 0.8660 0.0250 0.1923 0.7117 0.6919 77.1529 6.00 0.075 0.0120 0.8660 0.0250 0.1923 0.7117 0.6919 77.1529 6.00 0.075 0.0120 0.8660 0.0250 0.2537 0.9203 0.9556 93.1075 8.00 0.075 0.0120 0.8660 0.0250 0.2537 0.9203 0.9556 93.1075 8.00 0.075 0.0120 0.8660 0.0250 0.3103 1.0940 1.0000 57.4103 12.00 0.075 0.0120 0.8660 0.0250 0.3103 1.0940 1.0000 57.4103 12.00 0.075 0.0120 0.8660 0.0250 0.3103 1.0940 1.0000 57.4103 12.00 0.075 0.0120 0.9659 0.0250 0.4153 1.3762 1.0000 57.3359 2.00 0.075 0.0120 0.9659 0.0250 0.4153 1.3762 1.0000 50.3359 2.00 0.075 0.0120 0.9659 0.0250 0.4153 1.3762 1.0000 50.3359 2.00 0.075 0.0120 0.9659 0.0250 0.2444 0.3693 0.9550 94.1404 9.00 0.075 0.0120 0.9659 0.0250 0.2444 0.3693 0.9550 94.1404 9.00 0.075 0.0120 0.9659 0.0250 0.2444 0.3693 0.9550 94.1404 9.00 0.075 0.0120 0.9659 0.0250 0.2464 0.3693 0.9550 94.1404 9.00 0.075 0.0120 0.9659 0.0250 0.2466 1.0000 50.3702 0.9550 94.4272 9.00 0.075 0.0120 0.9652 0.0250 0.2466 1.0118 0.9950 94.4272 9.00 0.075 0.0120 0.9652 0.0250 0.2466 1.0118 0.9950 94.4272 9.00 0.075 0.0120 0.9962 0.0250 0.2500 0.2505 0.25	-	2 - 00	0.075	0-2120	0.5000	0.6250	0.14	54	0-3157	0.4049	49-16-4
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6.00 C.075 0.0120 0.6660 0.0250 0.2537 0.9203 0.9556 93.1075 8.00 C.(75 0.0120 0.8660 C.0250 0.3103 1.0940 1.0000 67.7947 10.00 C.075 0.0120 0.2660 C.0250 0.3640 1.2430 1.0000 57.4103 12.00 C.075 0.0120 0.8660 0.0250 0.4153 1.3762 1.0000 50.3509 2.00 C.075 0.0120 0.9659 C.0250 0.1172 0.4775 0.4099 51.9901 4.00 C.075 0.0120 0.9659 C.0250 0.1352 0.7655 0.6919 77.5931 6.00 C.075 0.0120 0.9659 C.0250 0.2444 0.9593 0.9556 94.1404 9.00 C.075 0.0120 0.9659 0.0250 0.2444 0.9593 0.9556 94.1404 9.00 C.075 0.0120 0.9659 C.0250 0.2444 0.9593 1.0000 69.01/2 10.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 55.0415 12.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 55.0415 12.00 C.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.9112		2.00	0.075	0.0120	0.8666	0.0250	0.12	214	0.4463	J-4099	51.5813
8.00 C.(75 0.0120 0.8660 C.(250 0.3103 1.0040 1.0000 67.7747 10.00 0.075 0.0120 0.6660 C.0250 0.3640 1.2430 1.0000 57.4103 12.00 6.075 0.0120 0.8660 0.0250 0.4153 1.3762 1.0000 50.3369 2.00 C.075 0.0120 0.9659 C.0250 0.1172 0.4775 0.4099 51.9901 4.00 C.075 0.0120 0.9659 C.0250 0.1852 0.7655 0.6919 77.8931 6.00 C.075 0.0120 0.9659 C.0250 0.2444 0.553 0.9550 94.1404 9.00 0.075 0.0120 0.9659 C.0250 0.2444 0.553 0.9550 94.1404 9.00 0.075 0.0120 0.9659 C.0250 0.2444 0.5693 0.9550 94.1404 9.00 0.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 69.01/2 10.00 0.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 50.0415 12.00 0.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.9112							0.19	23 .	0.7117	3.6714	77.1529
10.00 0.075 0.0120 0.8660 0.0250							0.29	37	0.4203	0.9526	93.1075
12.00 0.075 0.0120 0.8660 0.0250 0.4153 1.3762 1.0000 50.3369 2.00 0.075 0.0120 0.9659 0.0250 0.1172 0.4775 0.4099 51.9901 4.00 0.075 0.0120 0.9659 0.0250 0.1352 0.7655 0.6919 77.8931 6.00 0.075 0.0120 0.9659 0.0250 0.2444 0.9693 0.9556 94.1404 5.00 0.075 0.0120 0.9659 0.0250 0.2444 0.9693 0.9556 94.1404 5.00 0.075 0.0120 0.9659 0.0250 0.2349 1.3423 1.0000 69.01/2 10.00 0.075 0.0120 0.9659 0.0250 0.3499 1.3423 1.0000 55.0415 12.00 0.075 0.0120 0.9659 0.0250 0.3/92 1.4857 1.0000 51.9112 2.00 0.075 0.0120 0.9962 0.0250 0.1500 0.4673 0.4099 52.1175 4.00 0.075 0.0120 0.9962 0.0250 0.1532 0.7614 0.6919 76.0950 600 0.075 0.0120 0.9962 0.0250 0.1532 0.7614 0.6919 76.0950 600 0.075 0.0120 0.9962 0.0250 0.2416 1.0116 0.9555 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2416 1.0116 0.9555 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2416 1.0116 0.9555 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2952 1.2055 1.0000 69.37/2 10.00 0.075 0.0120 0.9962 0.0250 0.3459 1.3717 1.0000 59.2371											
2.00 0.075 0.0120 0.4659 0.0250 0.1172 0.4775 0.4099 51.9901 4.00 0.075 0.0120 0.9659 0.0250 0.1352 0.7655 0.6919 77.8931 6.00 0.075 0.0120 0.9659 0.0250 0.2444 0.9693 0.9556 94.1404 5.00 0.075 0.0120 0.9659 0.0260 0.2956 1.1788 1.0000 69.01/2 10.00 0.075 0.0120 0.9659 0.0260 0.3499 1.3423 1.0000 55.0415 12.00 0.075 0.0120 0.9659 0.0750 0.3792 1.4857 1.0000 51.9112 2.00 0.075 0.0120 0.9962 0.0250 0.1160 0.4673 0.4099 52.1176 4.00 0.075 0.0120 0.9962 0.0250 0.1532 0.7614 0.6919 76.0950 600 0.075 0.0120 0.9962 0.0250 0.1532 0.7614 0.6919 76.0950 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2416 1.0118 0.9556 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2952 1.2055 1.0000 69.37/2 10.00 0.075 0.0120 0.9962 0.0250 0.3459 1.3717 1.0000 59.2371											
4.00 C.075 0.0120 0.9659 C.0250 0.1352 0.7655 0.6919 77.8931 6.00 C.075 0.0120 0.9659 C.0250 0.2444 0.3693 0.9550 94.1454 5.00 C.075 0.0120 0.9659 0.0250 0.2956 1.1750 1.0000 69.0172 10.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 55.9415 12.00 C.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.9112 2.00 0.075 0.0120 0.9962 C.0250 0.1160 0.4673 0.4099 52.1175 4.00 C.075 0.0120 0.9962 C.0250 0.1532 0.7614 0.6919 76.0950 6.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0118 0.9555 94.4272 8.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.3772 10.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.3772	ı	12.00	0.075	0.0120	0.8660	0.0250	0.41	153	1.3762	1.0000	50.3309
4.00 C.075 0.0120 0.9659 C.0250 0.1352 0.7655 0.6919 77.8931 6.00 C.075 0.0120 0.9659 C.0250 0.2444 0.3693 0.9550 94.1454 5.00 C.075 0.0120 0.9659 0.0250 0.2956 1.1750 1.0000 69.0172 10.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 55.9415 12.00 C.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.9112 2.00 0.075 0.0120 0.9962 C.0250 0.1160 0.4673 0.4099 52.1175 4.00 C.075 0.0120 0.9962 C.0250 0.1532 0.7614 0.6919 76.0950 6.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0118 0.9555 94.4272 8.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.3772 10.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.3772		3.00	6 676	0.0110	0.4450	0 / 252		33	0 (22)		E 1 1212 : 1
6.00 C.075 0.0120 0.9659 C.0250 0.2444 0.9593 0.9556 94.1404 9.00 C.075 0.0120 0.9659 0.0250 0.2956 1.1788 1.0000 69.0172 10.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 52.0415 12.00 C.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.7112 2.00 0.075 0.0120 0.9962 C.0250 0.1160 0.4673 0.4099 52.1175 4.00 C.075 0.0120 0.9962 C.0250 0.1532 0.7614 0.6919 76.0950 6.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0118 0.9555 94.4272 8.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0118 0.9555 94.4272 8.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.37:2 10.00 C.075 0.0120 0.9962 C.0250 0.3459 1.3717 1.0000 59.2371											
9.00 C.075 0.0120 0.9659 0.0250 0.2956 1.1788 1.0000 69.0172 10.00 C.075 0.0120 0.9659 C.0250 0.3499 1.3423 1.0000 52.0415 12.00 C.075 0.0120 0.9659 C.0250 0.3792 1.4857 1.0000 51.7112 2.00 C.075 0.0120 0.9962 C.0250 0.1160 0.4673 0.4099 52.1175 4.00 C.075 0.0120 0.9962 C.0250 0.1532 0.7614 0.6919 76.0950 6.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0116 0.9555 94.4272 8.00 C.075 0.0120 0.9962 C.0250 0.2952 1.2055 1.0000 69.372 1.0000 69.2371 10.00 C.075 0.0120 0.9962 C.0250 0.3459 1.3717 1.0000 59.2371											
10.00 0.075 0.0120 0.9659 C.0250 0.3792 1.3423 1.0000 50.0415 12.00 0.075 0.0120 0.9659 C.0250 0.1160 0.4673 0.4099 52.1175 4.00 C.075 0.0120 0.9662 C.0250 0.1632 0.7614 0.6919 76.0950 6.00 C.075 0.0120 0.9662 C.0250 0.1632 0.7614 0.6919 76.0950 94.4292 8.00 C.075 0.0120 0.9662 C.0250 0.2416 1.0118 0.9555 94.4292 8.00 C.075 0.0120 0.9662 C.0250 0.2416 1.0118 0.9555 94.4292 10.00 C.075 0.0120 0.9662 C.0250 0.2952 1.2055 1.0000 69.37:2 10.00 C.075 0.0120 0.9662 C.0250 0.3459 1.3717 1.0000 59.2371											
2.00 0.075 0.0120 0.9659 (.0750 0.3792 1.4857 1.0000 51.7112 2.00 0.075 0.0120 0.9962 0.0250 0.1160 0.4673 0.4099 52.1175 4.00 0.075 0.0120 0.9962 0.0250 0.1532 0.7614 0.6919 76.0950 6.00 0.075 0.0120 0.9962 0.0250 0.2416 1.0118 0.9555 94.4272 8.00 0.075 0.0120 0.9962 0.0250 0.2952 1.2055 1.0000 69.37:2 10.00 0.075 0.0120 0.9962 0.0250 0.3459 1.3717 1.0000 59.2371											
2.00 0.075 0.0120 0.99&2 0.0250											
4.00 C.C75 0.0120 0.9962 C.C250		-2.00	0.019	0.9120	0.9619	(• 6 7 - 0	J • 3	776	1.7071	1.000	J & 0 7 L L L
4.00 C.C75 0.0120 0.9962 C.C250		2.00	0.075	0.0120	0.9962	0.4251	0.1	0.31	0.46.73	0.4099	52.1175
6.00 C.075 0.0120 0.9962 C.0250 0.2416 1.0118 0.9555 94.4272 8.00 C.075 0.0120 0.9962 0.0250 0.2952 1.2055 1.0000 67.37:2 10.00 C.075 0.0120 0.9962 C.0250 0.3459 1.3717 1.0000 59.2371											
8.00 (.075 0.0120 0.9962 0.0250 0.2952 1.2055 1.0000 69.37:2 10.00 (.075 0.0120 0.9962 0.0250 0.3459 1.3717 1.0000 59.2371					_						
10.00 (.675 0.0120 0.9962 6.6250 6.3459 1.371) 1.0000 59.23/1											
										1.0000	59.23/1
		12.00	0.675	0.0120	0.9962	1.6250	u.3	348	1.5160	1.0000	52.3443

FLOW	DIA. MAN	N. SUPFLY	CFAIN	DRAIN FLOW	ENTRY	NORMAL	PIPE LENGTH TO
L/S.	:M. COE	FF SLOPE	SLUPE	ENTRY DEPTH	ENERGY	· DEPTH	NORHAL DEPTH.
		(SIN)	(SIH)	RATIO H/D.	M _o	H/D.	L/D.
					<u> </u>		
						•	
2 - 00	0.075 0.0	120 0.2566	0.0167	0.1310	0.2102	0.4753	46.1400
	0.075 0.0			0.2913	0.3257	0.8110	63.7326
	0.075 0.0			0.3894	0.4116	1.0000	56.9000
	0.675 0.0			0.4812	0.4813	1.0000	44.4546
	0.675 0.0			0.5698	0.5388	1.0000	35.4055
	0.075 0.0			0.6548	0.5901	1.0000	27.7305
12.00	0.075 0.0	150 0.5300	(,,010)	0.0240	0.5901	1.0000	21.1309
2 60	0 075 0 3	130 0 6000	0 01/7	0 1454	A 2157		40 4025
	0.075 0.0			0.1454		0.4753	49.6925
	0.075 0.0			0.2316	0.4980	0.3110	69.6176
	0.075 0.0			0.3074		1.0000	64.7537
	0.075 (.)			0.3777	0.7511	1.0000	53.0033
	0.075 0.0			0.4446	0.0483	1.0000	46.0744
12.00	0.075 0.0	120 0.5000	C-0167	€.5093 ·	0.9326	1.0000	39.4850
	0.075 0.0			0.1296	0.3924	0.4753	51.2317
	C.075 0.3			0.2029	0.0232	0.8110	72.2718
	C.075 0.3			0.2722	0.5030	1.0000	66.3547
	0.075 0.0			0.3333	0.4533	1.0000	50.1776
	0.075 0.0			0.3918	1.0785	1.0000	51.0674
12.00	0.075 0.0	120 0.7070	0.0167	0.4475	1.1918	1.0000	45.0718
2.00	0.075 0.0	120 0.8666	0.0167	0.1214	0:4463	0.4753	52.1350
4.00	0.075 0.0	120 0.8660	C.C167	0.1923	0.7117	0.8110	75.5.36
6.00	6.675 0.0	120 0.6660	0.0157	0.2537	0.9203	1.0000	70.3122
8.00	0.075 0.0	120 0. 6660	0.0167	0.3103	1.0940	1.0000	60.5124
10.00	0.075 0.0	120 0.8660	0.0167	0.3540	1.2430	1.0000	53.8015
12.00	0.075 0.7	120 0.8660	0.0167	0.4153	1.37£2	1.0000	45 - 1232
2.00	0.075 0.0	120 0.9659	0.0167	0.1172	0.4775	0.4753	53.2288
4.00	0.075 0.1	120 0.5659	C.0167	0.1852	0.7555	0.8110	77.3659
	0.075 0.0			0.2444	0.9393	1.0000	71.3004
	0.675 0.3			6.2950	1.1768	1.0000	61.7246
10.00	0.675 0.0	120 0.9659	0.0167	0.3444	1.3423	1.0000	55.21+0
	0.075 0.0			0.3942	1.4857	1.0000	44.6831
2.00	0.075 0.0	120 0.9962	0.0167	. 0.1160	0.4073	0-4753	53.5474
	0.075 0.0			0.1332	0.7614	0.8110	77.5425
	0.675 0.0			0.2410	1.0118	1.0000	71.5000
	0.675 0.0			U.2952	1.2055	1.0000	62.0500
	0.075 0.0			0.3459	1.3719	1.0000	95.0130
	0.075 0.0			0.3948	1.5180	1.0000	50.1125
					-		, and the same of

								•	
į	FLOW	DIA .	MANN.	SUPPLY	DRAIN .	DRAIN FLCH	ENTRY	NURMAL	PIPE LENGTH TO
3	L/S.	h.	CUEFF	SLOPE	SLOPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL JEPTH.
				(SIN)	(SIN)	RATIO H/D.	Me	H/D.	L/D.
ì			•	(32,113	433				
									· ·
į									
I									
1			0.0120			0.1810	0.2102	0.5298	42.8450
	4.00	0.075	0.7120	0.2588	0.0125	0.2913	0.3257	0.9116	52.7000
	6.00	0.075	0.0120	U.2568	C. C125	U.3344	0.4116	1.0000	50.2423
ŀ	5.00	C.075	0.9120	0.2588	0.0125	0.4812	0.4813	1.0000	41.5263
	10.00	0.675	0.0120	0.2586	0.0125	U-5648	0.5388	1.0000	34.0004
			0.0120			0.6548	0.5901	1.0000	26.8996
l				•					
И	2 00	6 6.75	0.0120	0.5600	0.0125	0.1454	0.3157	0.5298	46.4392
Ŋ			0.0120				0.4980	0.9116	50.2478
Ņ						0.2316			
			0.0120			0.3074	0.0369	1.0000	57.9905
ŀ			0.0120			0.3777	0.7511	1.0000	51.0678
			0.0120			0.4446	0.0483	1.0000	44.0647
	12.00	0.075	0.7120	0.5000	0.0125	ú.5093	0.9326	1.0000	30.5196
							•		
j	2.00	0.675	0.0120	J.7070	0.0125	0.1298	0.3924	3.5298	40.2741
	4.00	0.075	0.0120	0.7670	0.0135	0.2059	0.0232	0.9116	60.7163
			6.0120			0.2722	0.5030	1.0000	61.5563
1			0.0120			0.3333	0.9533	1.0000	50.4110
			0.0120			0.3918	1.0785	1.0000	47.5045
l			0.0120			0.4475	1.1918	1.0000	44.0674
k	12.00	0.013	0.7125	0.7070	0.0123	0.4475	1.1710	1.0000	77.0017
I									
1	2 00	75							
			0.0120			0.1214	0.4463	0.5298	49.5530
ì			0.0120			0.1923	0.7117	0.9116	02.0371
1			0.0120			0.2537	0.9203	1.0000	63.5053
I			0.0150			0.3103	1.0940	1.0000	57.7350
			0.0120			0.3640	1.2439	1.0000	52.2223
į	12.00	0.675	0.0120	0.8666	0.0125	0.4153	1.3762	1.0000	47.1024
ž									
K									
	2.00	C. 675	0.3120	0.9659	C.6125	U. 1172	0.4775	0.5248	50.1315
			0.0120			0.1852	0.7655	0.9116	04.7154
			0.0120			0.2444	0.7393	1.0000	64.4575
			6.3120			0.2956	1.1785	1.0000	50.1357
5			0.1120			0.3499	1.3423	1.0000	53.6323
-			6.0120			0.3992	1.4057	1.0000	40.7571
	2200			00,007		0 6 3 7 7 2	201031	2.0000	100,372
1									
I	2 00	£ 075	0.0120	0.0643	0 0135	(31(0	0 6473	0 5308	5, 37/ =
1							0.4873	0.5298	56.3745
1			0.0120			0.1032	0.7514	0.7116	62.9053
			0.0120			0.2416	1.0110	1.0000	64.7500
			0.0123			0.2472	1.2055	1.0000	54.29.7
			0.0120			6.3454	1.3719	1.0000	54.7271
	12.00	0.675	0.0120	2.4962	0.6125	0.3745	1.5180	1.0000	49.0527
all.									

					•			
FLOW	DIA.	HANN.	SUPPLY	GRAIN "	DRAIN FLOW	ENTRY	NORHAL	PIPE LENGTH
L/S	N.	COEFF	SLOPE	SLOPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPT
			(SIN)	(SIN)	RATIO H/D.	ri.	H/D.	L/0.
				•				
2.00	0.075	0.0150	0.2586	0.0500	0-2103	0.1614	0.3743	25.2949
4.00	0.075	0.0150	0.2588	0.0500	0.3411	0.2471	0.6284	36.4986
6.00	0.075	0.9150	0.2566	0.6500	0.4567	0.3100	0-8647	46.9254
			0.2588		0.5695	0.3602	1.0000	34.1350
10.00	0.075	0.0150	0.2568	0.0500	0.6753	0.4029	1.0000	21.5631
12.00	0.075	0.0150	0.2588	C.0500	0.7806	0.4391	1.0000	14.1641
			1,					
2.00	0.075	0.3150	0.5000	0.0500	0.1686	0.2394	0.3743	28.1506
			0.5000		0.2703	0.3731	0.6284	43.0255
6.00	0.075	0.0150	0.5000	0.0500	0.3606	0.4730	0.8647	52.7245
8.00	0.075	0.0150	0.5000	0.0500	0.4446	0.5549	1.0000	41.1453
			0.5000		0.5249	0.0240	1.0000	24.3543
			0.5000		0.6040	0.6811	1.0000	22.6614
		,						
								•
2.00	0.075	0.2150	0.7070	C.0500	0.1503	0.2966	0.3743	29.3730
			0.7070		0.2399	0.4659	0.6284	45.0014
			0.7070		0.3106	0.5952	0.8647	55.3296
			0.7670		0.3918	0.7008	1.0000	44.3932
			9.7070		0.4617	0.7904	1.0000	33.0452
			0.7070		8555.0	0.8692	1.0000	26.7842
					•			
2.00	0.075	0.9150	0.8660	0.0500	0.1405	0.3369	0.3743	30.0179
			0.8660		0.2238	0.5316	0.6254	40.0559
			0.8660		0.2966	0.6813	0.8647	56.7205
			0.86.9		0.3640	0.3053	1.0000	40.1728
			0.6660		0.4200	0.9116	1.0000	35.0865
			0.6666		0.4897	1.0035	1.0000	29.0425
							•	
2.00	0.075	0.C150	0.9659	C. 05 00	0.1356	0.3605	0-3743	30.3385
			0.9659		0.2155	0.5714	0.6254	46.6006
			0.9659		0.2854	0.7334	0.8647	57.4335
8.00	0.075	0.0150	0.9659	0.6500	0.3449	0.2625	1.0000	47.0947
			0.9659		0.4114	0.9827	1.0000	30.1150
			0.9659		0.4705	1.0833	1.0000	30.1873
2.00	0.075	0.0150	0.9962	0.0500	0.1342	0.3681	0.3743	30-4343
			0.9962		0.2133	0.5827	0.6284	46.7449
6.00	0.075	0.0150	0.9962	0.0500	0.2320	0.7505	0.8647	57.6573
			0.9962		0.3459	0.5374	1.0000	47.3508
10.00	0.075	0.9150	0.9962	0.0500	U. 4005	1.0054	1.0000	30.4204
12.00	6.075	0.0150	0.9962	0.0500	0.4051	1.1073	1.0000	30.5090

* }						•		
FLOW	DIA.	MANN.	SUPFLY	CPAIN	DRAIN FLUH	ENTRY	NORMAL	PIPE LENGTH TO
		CJEFF		SLUPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPTH.
LIS.	*•	CUEFF					_	
			(SIN)	(SIN)	RATIO H/L.	n.	H/D.	L/D.
								•
							÷.	
	.:							
2.00	0-075	0.0150	0.2568	0.0250	0.2103	0.1614	0-4632	27.6673
			0.2586		0.3411	0.2471	0.8257	37.3750
			0.2588		0.4587	0.3100	1.0000	31.7551
			0.2588		0.5698	0.3602	1.0000	23.6725
10.00	0.675	0.9150	0.2566	0.0250	0.6703	0.4029	1.0000	17.5447
12.00	0-6.75	0.0150	0.2560	C-C250	0.7808	0.4391	1.0000	12.1973
	000.7	00020	002300					
							•	
			Ė					
			0.5000		0.1056	0.2394	0.4832	30.2307
4.00	C.075	0.0150	0.5000	C.6250	0.2703	0.3731	0.8257	41.5546
			0.5000		0.3606	0.4730	1.0000	37.2575
			0.5000		0.4446	0.5549	1.0000	30.1712
			0.5000		0.5249	0.0240	1.0000	24.5314
12.00	0.075	0.7150	0.5000	C.0250	0.0040	0.5811	1.0000	20.1304
		•						
7 00	0 175	0 0163	0 7676	0.0250	6 1503	0 2044	0 4033	21 (6)
			0.7070		0.1503	0.2966	0.4832	31.4041
4.00	0.075	0.0150	0.7070	n. U250	0.2349	0.4659	0.8257	43.4919
6.00	C. 075	0.0150	0.7070	C. 0250	0.3106	0.5952	1.0000	39.3237
			0.7070		0.3916	0.7005	1.0000	33.2589
			9.7076		0.4617	0.7904	1.0000	26.3351
12.00	0.075	0.9150	0.7070	0.0250	0.5298	0.4692	1.0000	24.0525
6								
1.								
2.00	0.075	0-0150	0.8660	0 - 6250	0.1405	0.3369	0.4532	32.0373
			0.6666		0.2238	0.5315	0.8257	44.5475
			0.8666		0.2966	0.6613	1.0000	41.2502
			0.86.0		J. 3640	0.8053	1.0000	34.9662
10.00	0.075	6.0150	0.2660	0.0250	0.4260	0.4116	1.0000	36.3131
			0.8660		0.4847	1.0038	1.0000	20.2015
1		007270	3 4 5 6 6 6	3602 70	00 10 / 1	200000	10000	20020,7
§								
		_						
			0.9659		0.1350	0.3605	0.4832	32.3551
4.00	0.675	6.0150	0.9659	0.0250	0.2155	0.5714	0.8257	45.0930
			0.9659		U • 2354	0.7334	1.0000	42.0015
			0.4659		0.3449	0.3685	1.0000	30.0000
			0.9654		0.4114	0.9827	1.0000	31.3124
12.00	0.675	0.7150	0.9654	C.0250	0.4705	1.0833	1.0000	63169
ŧ								
2.00	0-176	0-0150	0.9962	0.0250	0.1342	0.3681	0-4832	36.4517
			0.9962		0-2133	0.2027	0.62>7	45.2444
			0.4962		0.2520	0.7505	1-0000	42.2207
			0.9962		0.3459	0-4874	1.0000	30.1003
			0.5462		0.4905	1.0054	1.0000	31.0104
			0.9962		0.4051	1.1073	1.0000	27.0173
12.00	(00 1)	0.3130	0.7762	0.0250	U. TO J L	1.1073	7 9 00 0	2100.10

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIH)	CPAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY no	MORMAL DEPTH H/D:	PIPE LENGTH NORMAL DEPT L/D.
4.00 6.00 8.00 10.00	0.075 0.075 0.075 0.075	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.2588 0.2588 0.2588	0.0167 C.0167 C.0167 G.0167	0.2103 0.3411 0.4587 0.5698 0.6763 0.7808	0.1614 0.2471 0.3100 0.3602 0.4029 0.4391	0.5630 0.9712 1.0000 1.0000 1.0000	23.0455 23.4572 27.1040 21.7743 10.5550 11.6657
4.00 6.00 3.00 10.00	0.075 0.075 0.075 0.075	0.0150 0.0150 0.0150 0.0150 0.0150	0.5000 0.5000 0.5000 0.5000	0.0157 0.0157 0.0157 0.0167	0.1660 0.2703 0.3606 0.4446 0.5249 0.6040	0.2394 0.3731 0.4730 0.5549 0.6240 0.6811	0.5630 0.9712 1.0000 1.0000 1.0000	25.6075 25.2314 32.4463 20.1049 23.6846 19.4231
4.00 6.00 8.00 10.00	0.075 0.075 0.075 0.675	0.0150 0.0150 0.0150 0.0150 0.0150	0.7070 9.7070 0.7070 0.7070	0.0167 0.0157 0.0167 0.0167	0.1503 0.2399 0.3186 0.3918 0.4617	0.2966 0.4659 0.5952 0.7008 0.7904 0.8692	0.5630 0.9712 1.0000 1.0000 1.0000	26.8014 22.2352 35.0068 31.1552 27.1433 23.3270
4.00 6.00 8.00 10.00	0.075 C.075 O.075 O.075	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.660 0.665 0.665 0.665	0.0157 0.0167 0.0167 0.0167	0.1405 0.2230 0.2906 0.3640 0.4230 0.4897	0.3369 0.5316 0.6513 0.3053 0.4116 1.0038	0.5630 0.9712 1.0000 1.0000 1.0000	27.4506 34.7112 36.4031 32.8464 29.09.2 25.4914
4.00 6.00 8.00 10.00	0.075 0.075 0.075 0.075	0.0150 0.0150 0.0150 0.0150 0.0150	0.5659 0.9659 0.9659 0.9659	C.0167 O.0167 C.0167 C.0157	- 0.1356 0.2155 0.2354 0.3499 0.4114 0.4705	0.3605 0.5714 0.7334 0.4685 0.9527 1.0833	0.5630 0.9712 1.0000 1.0000 1.0000	27.7777 72.5963 37.1311 33.72=1 30.0390 26.5943
4.00 6.00 8.00 10.00	0.075 0.075 0.075 0.075	0.0150 0.0150 0.0150 0.0150 0.0150	0.9962 0.9962 0.9962 0.9962	0.0167 0.0167 0.0167 0.0167	0.1342 0.2133 0.2520 0.3459 0.4065	0.3681 0.5827 0.7505 0.3874 1.0054 1.1073	0.5630 0.9712 1.0000 1.0000 1.0000	27.5759 57.7440 37.3542 33.9738 30.3543 26.9003

FLO		DIA.	MANN.	SUPPLY		DRAIN FLOW	ENTRY	NORMAL	PIPE LENGTH TE
LIS	•	M.	COEFF	SLOPE	SLUPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPTH.
				[412]	(SIN)	RATIC H/C.	M.	H/D.	L/3.
1									
1 2	00	0.75	0 0150	0.2566	0 0125	0.2103	0.1614	0.6204	6.5779
111				0.2568		0.3411	0.2471	1.0000	22.6261
F 17				0.2566		0.4587	0.3100	1.0000	25.4236
				0.2560		0.5676	0.3602	1.0000	20.9417
				0.2565		0.6763	0.4029	1.0000	16.1022
				0.2580		6.7 308	0.4391	1.0000	11.4143
12.0	•		0. 3130	002 300	0.0123	0. 7000	021371	20000	22012.0
1									
2.	00	0.075	0.0150	0.5000	0.0125	0.1656	0.2394	0.6204	16.9057
7.5				0.5000		0.2703	0.3731	1.0000	26.7413
2 -				0.5000		0.3600	0.4730	1.0000	30.7075
				0.5000		U.4446	0.5549	1.0000	27.2973
10.	00	0.075	0.0150	0.5000	0.0125	0.524+	0.0240	1.0000	23.1525
12.	00	0.075	0.0150	0.5000	0.0125	0.6040	0.0811	1.0000	17.0427
N									
2.	00	0.075	0.0150	0.7070	0.0125	0.1503	0.2966	0.6284	17.4976
4.	00	0.075	0.3150	0.7076	0.0125	0.2399	0.4659	1.0000	28.7257
1.1				0.7076		0.3186	0.5952	1.0000	33.2500
				0.7076		0.3918	0.7003	1.0000	30.2323
1.6				0.7676		0.4517	0.7904	1.0000	26.5855
12.	0υ	C.075	0.0150	0.7070	0.0125	0.52o8	0.0692	1.0000	22.9552
				0.6660		0.1405	0.3369	0.6204	18.3403
				0.8660		0.2238	0.5316	1.0000	29.8342
				0.8660		0.2966	0.6813	1.0000	34.5390
				0.8660		0.3640	0.8353	1.0000	31.9146
				0.2660		0.4250	0.9116	1.00.0	28.53.7
1150	50	C.0 /5	0.0190	0.2960	0.0125	04397	1.0038	1.0000	25.1193
1									
2.	0.0	0.075	0-0150	0.9659	0.0125	0.1356	0.3605	0.6204	19.1724
				0.9659		0.2155	0.5714	1.0000	30.4167
				0.9659		0.2354	0.7334	1.0000	35.3537
4				0.4654		0.3419	0.0685	1.0000	34.74.3
				0.4154		0.4114	0.9527	1.0000	29.5171
				0.9655		0.4765	1.0333	1.0000	26.2179
2.	0.0	0.075	0.0150	0.9962	C. 0125	0.1342	0.3681	0.6204	19.5473
				0.9462		0.2133	0.5827	1.0000	30.5727
				0.9962		0.2520	0.7505	1.0000	35.5534
				0.9912		0.3459	0.3074	1.0000	35.0373
				0.9962		0.4005	150054	1.0000	24.0154
12.	00	0.675	6.0150	0.9964	(.6125	0.4651	1.1073	1.0000	26.5233

						•		1
FLOW	DIA.	MANN.	SUPPLY	DRAIN	DRAIN FLOW	ENTRY	NORMAL	PIPE LENGTH 1
L/S.	M.		SLOPE		ENTRY DEPTH		DEPTH	NORHAL UEPTH.
2,,,,		000.1	(SIN)		RATIO H/D.	Ma.	H/0.	L/D.
			12741	13741	KAIIO M/U.	110	11/00	270.
								- 1
						,		
				•				- //
								- 1
2 - 00	12075	0-0130	0.2585	0.0500	0.2384	0.1312	0.4280	18.0963
			0.2588		0.3894	0.1992	0.7241	25.8504
			0.2588		0.5259			
						0.2491	1.0000.	31.1132
			3335.0		0.6548		1.0000	15.8033
			0.2588		U.7808		1.0000	
12.00	0.075	0.0130	0.2568	0.0500	0.9028	0.3523	1.0000	5.7300
								1
								1
2-00	0.075	0.0130	0.5000	0.0500	0.1906	0.1917	0.4280	20.1423
			0.5000		0.3074	0.2959	0.7241	29.0764
			0.5000		0.4114	0.3735	1.0000	36.3344
								100
			0.5000		0.5093	0.4357	1.0000	20.6052
			0.5000		0.6040	0.4868	1.0000	15.4670
12.00	0.075	0.3130	0.5000	C-0500	0.6948	0.5326	1.0000	11.5412
						•		
2.00	0.075	0.0110	0.7070	0.0500	0.1696	0.2368	0.4290	21.0638
			0.7670		0.2722	0.3682	0.7241	30.5722
			0.7676		0.3630	0.4672	1.0000	36.8032
			0.7070		0.4475	0.5484	1.0000	22.9777
								100
			0.7070		0.5288	0.0157	1.0000	10.1600
12.00	0.075	6.7130	0.7070	C. 0500	0.6079	0.6733	1.0000	14.4672
2.00	0.075	C-0130	0.8660	C.0500	0.1586	0.2682	0.4280	21.5576
4.00	0.075	C.0130	0.8660	0.0500	0.2537	0.4196	0.7241	31.3847
6.00	0.075	0.0130	0.8666	0.0500	0.3372	0.5354	1.0000	40.1904
			0.84.0		0.41>3	0.0289	1.0000	24.2934
			0.8660		0.4877	0.7083	1.0030	14.6675
			0.8660		0.5620	0.7765	1.0000	15.1354
12.00	01017	0.0130	0.0000	5 6 5 5 5 5	0.7020	34.107	20000	2002374
3 00	0 675	0 6110	0.0450	C 05.00	0 1530	0 3240	0 62 0	21 90 4
			0.9659		0.1530	0.2869	0.4230	21.8054
			0.9659		0.2444	0.4499	0.7241	31.7962
			0.9659		0.3245	0.5752	1.0000	40.5321
			0.9659		0.3972	0.5770	1.0000	24.9652
10.00	C.075	0.0130	0.9659	0.0500	0.4705	0.7631	1.0000	20.4335
12.00	0.075	0.0130	0.4659	0.0500	U.5376	0.0373	1.0000	16.9527
2.00	0.675	0.0130	0.9962	0-0500	0.1512	0.2930	0.4230	21.8540
			0.9962		0.2416	0.4593	0.7241	31. 9215
			0.9962		0.3210	0.2867	1.0000	41.0575
						0.6911		
			0.9962		0.3945		1.0000	25.1514
			0.9962		0.4651	0.7796	1.0000	20.6502
12.00	0.075	0.3130	0.9962	0.6560	0.5337	0.5544	1.0000	17.2071

F	LOW	DIA.	MANN.	SUPPLY	DFAIN	DRAIN	FLCH	ENTRY	NORMAL	PIPE LENGTH TE
	15.	· P.	CHEFF	SLI PE	SLUPF	ENTRY	HT936	ENERGY	DEPTH	NORMAL DEPTH.
				(SIN)	(SIN)	RATIO	H/U	N.	H/J.	L/D.
									-	
-										
10	2 00	A. 675	6 0130	0.2588	0.0250	0 - 23	44	0.1312	0.5542	15.5035
1				0.2528		0.35		0.1992	0. 4556	14.5247
1				0.2526		(• 52		0.2491	1.0000	10.3700
						0.65		0.2895	1.0000	12.7453
				0.2560				0.2845	1.0000	8.7551
1				0.2568		0.78			1.0000	
4	2.00	C.075	0.7130	0.2586	0.0250	0.90	20	0.3523	1.0050	0.1641
	2 00	0 075		0 5 6 6 6	0 6355	0.10	0.7	0 1017		17 (2)2
j				0.5000		0.19		0.1917	0.5542	17.4220
			-	0.5000		0.30		0.2959	0.9556	20.4574
1				0.5000		0.41		0.3735	1.0000	20.7414
ш				0.5000		0.50		0.4357	1.0000	17.2355
				0.5000		0.60		0.4368	1.0000	13.7744
1	2.00	0.075	0.0136	0.5000	C-4250	0.69	45	0.5325	1.0000	10.5843
п								•		
П										
М				0.7070		0.16		0.2368	0.5542	10.3434
и				0.7676		0.27		0.3682	0.9556	21.0553
П				0.7070		C • 35		0.4672	1-0000	22.0453
И				0.7076		0.44		0.5484	1.0000	19.5114
				0.7070		0.52		0.0157	1.0000	10.3005
1	12.00	0.675	0.0130	0.7676	0.0250	0.60	179	0.0733	1.0000	13.3952
И					•					
И										
И				0.8660		0.15		0.2682	U-5542	16.8434
М				0.5466		6.25		0.4190	0.9520	21.5495 .
П	6.00	0.675	0.9130	0.8666	0.6250	0.33	72	0.5354	1.0000	23.7257
П				0.8666		0.41		0.6289	1.0000	20.7525
1	0.00	C.675	0.0130	0.8666	0.0250	⊍ • 4 3		0.7083	1.0000	17.3210
1	12.00	0.075	0.0130	0.5660	0.6250	0.56	20	0.7765	1.0000	15.0123
				0.9654		U - 15		0.2569	J. 3542	14.6933
				0.9659		0.24	44	0.4499	J. 9356	21.3423
					0.0250	U.32		0.5752	1.0000	24.2700
	8.00	C.L75	0.7100	0.4654	C.0250	U.34	92	0.6770	1.0000	21.4357
1	10.00	C. 675	0.1130	0.9659	C.0350	0-47	U 5	0.7631	1.30.0	10.5057
1	12.00	6.075	0.0180	0.9659	0.6250	0.53	90	0.0373	1.0000	15.5373
	2.00	0.675	0.0130	0.9962	C+0250	C. 15	12	0.2930	0.5542	14.1700
	4.00	0.075	0.7111	0.4962	0.0250	6.24	16	0.4540	U. 9556	21.9312
	0.00	0.075	0.0140	0.9462	C.0250	0.32	10	0.9867	1.0000	24.41:2
	4.00	(.675	0.0139	0.9962	0.0250	0.39	140	0.6911	1.0000	21.5234
1	10.00	C.C75	U- 11:0	0.4962	0.6250	0.45		0.7735	1.0000	13.77//
	12.60	0.075	0.1110	0.4962	0.0250	0.53		0.0544	1.0000	16.0501

	•				* *			
FLOW	DIA.		SUPPLY		DRAIN FLOW		. NORMAL	PIPE LENGTH
L/S.	N.	COEFF	SLOPE		ENTRY DEPTH	ENERGY	DEPTH	NORHAL DEPT
			(SIN)	(21H)	RATIO H/D.	M.	H/D.	L/0.
•	*		•					
					•	•	•	
	ingt.							·
	17							
2.00	0.075	0.0130	0.2588	0.0167	0.2384	0.1312	0.6470	2.4537
4.00	0.075	0.0130	0.2568	0.0167	0.3894	0.1992	1.0000	13.9947
6.00	0.075	0.0130	0.2568	0.0157	0.5259	0.2491	1.0000	15.3240
6.00	0.075	0.9130	0.2586	C.0167	0.6548	0.2896	1.0000	12.0116
10.00	0.075	0.3140	0.2588	0.0167	0.7808	228 د ٠	1.0000	0.4164
12.00	0.075	0.0130	3325.0	C-U167	1 0.9028	0.3523	1.0000	5.0115
				,				
2.00	0-075	0.0190	0.5000	0-0167	0.1906	0.1917	0.6470	8.8134
		0.0130			0.3074	0.2959	1.0000	16.9502
		C.0130			0.4114	0.3735	1.0000	19.1147
		0.3130			0.5093	0.4357	1.0000	16.4009
		0.0150			0.6040	0.4351	1.0000	13.3035
		0.0130			0.6948	0.7325	1.0000	10.3037
12.00	0.075	0.7533	0.5000	0.0107	0.0740	0.5325	1.5000	10.3037
2 00	0 075	0.0340	0 7676	0.01/7	6 24 14	0 22/4	0 (1 7 0	6 20 5
		0.0180			0.1676	0.2368	0.6470	9-2045
		0.0130			0.2722	0.3682	1.0000	18.4214
		0.0130			0.3630	0.4672	1.0000	20.9941
		0.0130			0.4475	0.5484	1.0000	10.6545
		0.3130			0.5288	0.6157	1.0000	15.8610
12.00	0.075	0.0130	0.7070	0.0167	0.6079	0.6733	1.0000	13.0784
					,			
		0.0130			0.1506	0.2682	0.6470	9.3122
		0.9130				0.4196	1.0000	14.2442
		0.0130			U • 3372	0.5354	1-0000	22.0631
		0.0130			0.4153	0.6289	1.0000	19.9131
		0.0140				0.7083	1.0000	17.3013
12.00	0.075	0.7130	0.8660	0.6167	0.5620	0.7765	1.0000	14.6792
2.00	0.075	0.0130	0.9659	0.0167	0.1530	0.2869	0.6470	9.3341
4.00	0.075	0.0130	0.9659	6.6167	0.2444	0.4499	1.0000	14.6603
6.00	0.075	0.0130	0.9659	C. L157	0.3245	0.5752	1.0000	22.0026
8.00	0.675	0.0139	0.9659	0.0167	0.3942	0.0779	1.0000	20.5635
10.00	0.075	0.0130	0.4659	0.0167	0.4705	0.7631	1.0000	18.0410
		0.0140			0.5346	0.8373	1.0000	15.4973
2.00	0.675	0.0180	2.5562	0.0167	G-1512	0.2930	0.6470	4.3346
		0.0130			0.2416	0.4598	1.0000	14.7904
		0.0130			0.3210	0.5867	1.0000	26.7476
		0.0130			0.3946	0.5911	1.0000	20.7436
		0.7130		_	0.4651	0.7796	1.0000	10.2533
		0.0130			0.5337	0.0544	1.0000	15.7141
12.00	0.075	0.01730	0.7762	0.0101	007331	0 8 7 2 T T	1.0000	470111

FLOW	DIA.	MANN. CUEFF	STOPF (21H)	DRAIN SLCPE (SIN)	DRAIN FLOH ENTRY DEPTH SATIO H/D.	ENTRY ENERGY M.	NURMAL HT93U H/O-	PIPE LENGT NOKMAL JEP L/D.
4.00 6.00 8.00 10.00	0.100 0.100 0.100	0.0070 0.0070 0.0070 0.0070 0.0070	0.2568 0.2568 0.2568 0.2568	0.0500 0.0500 0.0500 0.0500	0.0906 0.1422 0.1364 0.2267 0.2644 0.305	0.2566 0.4174 0.5467 0.6575 0.7555	0.1549 0.2478 0.3243 0.4050 0.4775 0.54d3	34.5574 55.9953 75.3511 94.2911 109.7734 124.0754
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0070 0.0070 0.0070 0.0070 0.0070	0.5000 0.5000 0.5000	0.0500 0.0500 0.0500 0.0500	0.0737 0.1148 0.1495 0.1813 0.2108 0.2369	0.3830 0.6302 0.6355 1.0108 1.1679 1.3099	0.1549 0.2470 0.3243 0.4050 0.4778 0.5403	30.9270 65.7402 67.4115 105.3044 122.5377 136.44J0
4.00 6.00 8.00 10.00	C.100 C.100 C.100	0.0090 0.0090 0.0090 0.0090 0.0090	0.7070 0.7070 0.7070 0.7070	0.0500 0.0500 0.0500 0.0500	0.0660 0.1026 0.1334 0.1615 0.1674 0.2120	0.4749 0.7849 1.0441 1.2668 1.4704 1.6537	0.1549 0.2478 0.3243 0.4050 0.4778 0.5483	40.5040 60.3774 90.9339 109.6439 127.6413 144.2115
4.00 6.00 8.00 10.00	0.100 0.100 0.100 C.100	0.0070 0.0070 0.0070 0.0070 0.0070	0.86cC 0.86cC 0.86cC 0.66cC	0.0500 0.0500 0.0500 0.0500	0.0620 0.0961 0.1249 0.1510 0.1752 0.1979	0.5374 0.6921 1.1591 1.4457 1.6785 1.5942	0.1549 0.2473 0.3293 0.4050 0.4778 0.5483	41.2826 69.7013 92.7224 111.8750 130.2163 147.1742
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0090 0.0090 0.0090 0.0090 0.0090	0.9659 0.9659 0.9659	0.0500 0.0500 0.0500 0.0500	0.0505 0.0928 0.1205 0.1456 0.1538 0.1908	0.5752 0.9555 1.2748 1.5526 1.5052 2.0352	0.1549 0.2478 0.3293 0.4050 0.4778 0.5453	41.6779 70.3539 93.6111 112.9935 131.5349 146.6333
4.00 6.00 8.00 10.00	0.100 0.160 0.100 0.100	0.5090 0.0090 0.0090 0.0090 0.0090	0.5962 0.9962 0.9962	0.6500 0.6500 0.6500 0.6500	0.0593 0.0919 0.1173 0.1442 0.1671 0.168	0.5858 0.7757 1.3006 1.5834 1.8418 2.0770	0.1549 0.2473 0.3243 0.4050 0.4778 0.5453	41.77±0 70.5521 93.35±3 113.2957 131.6432 144.0431

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FLOH	DIA.		SUPPLY		DRAIN I		ENTRY	NORMAL	PIPE LENGTH TO
L/5.	. H.	CJEFF	SLUPE	SLUPE	ENTRY I	_		DEPTH	NORHAL DEPTH.
	•		(ZIM)	(SIH)	OITAP	H/U.	ಗ •	H/U.	L/D.
	•								
									•
2.00	0.100	0.0090	0.2568	0.0250	0.09	08	0.2566	0-1954	46.2220
4.00	0.100	0.2272	3.2566	0.0250	0.14	22	0.4174	0.3157	79.0829
			0.2560		6.13	54	0.5467	0.4231	103.9569
			0.2586		0.220	0 7	0.0575	0.5239	124.1655
			0.2586		v.26		0.7555	0.6216	142.9213
			0.2560		0.30		0.0425	0.7103	150.4177
				•					
2.00	0.100	0.0000	0.5000	0-0250	0.07	37	0.3830	0.1954	51.5902
			0.5666		U.114		0.6302	0.3157	84.7493
			0.5000		0.14		0.0302	0.4231	111.6337
			0.5000		0.18		1.0105	0.5239	133.5376
									153.5575
			0.5000		0.21		1.1679	3.6216	
12.00	0.100	0.0090	0.5000	0.0250	ũ. 23	5 9 .	1.3099	0.71n3	170.8308
					•				
		_	0.7076		0.06		0.4749	0.1954	53.0057
			0.7076		0.10.		0.7649	0.3157	87.1523
			0.7076		U.13		1.6441	0.4231	114.3755
			0.7076		0.16		1.2663	J.5239	137.0047
			0.7070		· 13		1.4704	0.6216	150.5157
12.00	C-100	0.1030	3.7070	(250	U.21	20	1.6537	0.7163	176.2345
			0.6660		0.06	20	0.5374	J. 1954	53.7242
4.00	C-100	0.0070	0.8740	0.0250	0.09	61	0.3921	0.3157	86.4023
6.00	0.100	0.0000	0.8660	C • C250	0.12	49	1.1391	0.4231	116.55:1
8.00	0.160	0.0000	0.8166	0.6250	0.15	10	1.4457	U.5239	139.7161
10.06	C.100	C. 2010	0.6666	0.0250	0.17	o 2	1.6785	0.6216	161.0579
12.00	0.100	0.3070	0.8660	C.0250	6.19	79	1.3942	0.7103	174.0773
				•					
2.00	0.100	0.0000	0.9654	C.0250	0.05	43	0.5752	Ú-1954	54.0934
4.00	0.100	0.3070	0.4659	C.C250	0.09	25	0.9555	0.3157	89.0295
6.00	6.100	0.0040	0.4659	C . 0250	0.12			0.4231	117.41++
			0.9659		Ü.14			0.5234	140.7013
			0.9659		0.10			0.0216	162.3401
			0.9654		0.1+		2.0352	J.7103	180.4453
		20,9	,						
2-110	0.100	U-2030	0.994	0.6250	. 4.05	43	0.5.58	0.1954	54.1952
				(.0250				0.3157	69.2143
			0.4962		0.07			0.4231	117.65>3
			0.9964		0.14			0.5239	
			0.9964		U.lo			3.5216	102.0-1/
			0.9462						
	0.100	0. 10.70	11-1402	(• 0 % 5 3	U.18	90	2.0770	0.7153	180.55/1

	0									
FL		DIA.	MANN.	SUPPLY		GRAIN FLOH	ENTRY	NORMAL	PIPE LENGTH	1
L	5.	M.	COEFF	SLOPE	STCAE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL SEPT	:
				CSINI	(814)	RATIO H/D.	A.	H/0.	L/D.	
							•	•		
										1
										а
2	0.0	6 100	0.7090	0.2599	0 0167	0.0908	0.2566	0.2242	55.3242	1
			0.0070			G.1422	0.4174	0.3645	80.3575	1
			0.0010			0.1864	0.5467	0.4917	116.6239	1
			0.0000			0.2207	0.6575	0.6109	136.5984	1
	-		0.00+0			2644	0.7555	0.7271	155.0115	1
			0.0030			0.3005	0.0425	0.8403	164.9513	
_										1
										1
2.	.00	C.100	0.0090	0.5000	0.0167	0.0737	0.3830	0.2242	58.5317	
			0.0000		_	0.1148	0.6302	0.3645	94.3193	1
			0.0090			0.1495	0.8355	0.4917	124.0119	1
			0.7970			0.1813	1.0105	0.6108	145.7409	1
			0.0090			0 • 21 úd	1.1679	0.7271	165.6941	Ш
12	.00	0-100	0.0090	0.5000	C.0167	0.2339	1.3099	0.8403	162.1046	П
										н
2	6.0	0 100	0.0000	0 7070	0 63 63	0.0440	0 (3/0	0 33/3	50 0177	1
			0.0090 0.0090			0.0660	0.4749	0.2242	59°9177 96°6954	ı
			0.0070			0.1026 U.1334	0.7849	0.4917	127.2047	1
			0.0090			0.1615	1.2663	0.4917	149.7349	1
			0.3090			0.1874	1.4704	0.7271	170.4153	1
			0.0070			0.2120	1.6537	0.8403	167.4975	Ł
		00200	0.00,3	001010	,	0.2120	200001	0 8 0 10 3	2014 1717	L
					•					п
2	. 00	0.100	G.0030	0.8660	0.6167	0.0620	0.5374 .	0.2242	60.6230	ı
4	.00	0.100	U. 3090	0.8660	0.0157	0.0961 .	0.0921	0.3645	97.9343	1
6	.00	0.100	6.0070	0.8666	C.0167	0.1249	1.1891	0.4917	125.8341	ш
			0.0070			0.1510	1.4457	0.6108	153.1153	1
			0.0070				1.6785	0.7271	155.6619	ı
12.	.00	0.100	0.0040	0.8660	0.0167	0.1979	1.8942	0.8403	170.0025	ш
2	0.0	0 100	0 2030	0 6456	0 0147	0.0509	0 6757	0 2242	40 0043	
			0.2073			0.0598 0.0928	0.5752 0.4555	0.2242	60.9943 98.5559	
			0.1090				1.2745	0.4917	126.9151	П
			0.7070				1.5525	0.6103	156.8503	н
			0.0090				1.3052	0.7271	142.6715	п
			0.0090			0.1908	2.0352	0.8403	174.9530	п
		00200		•••••						н
2.	-00	0.100	0.0040	0.9962	0.0167	0.0593	0.5658	0.2242	61.0893	
			0.0090			0.0919	0.4757	0.3645		
			0.0090				1.3006	0.4917	128.8254	
			0.0070				1.5839	0.6108	157.8817	
			0.0000				1.8415	0.7271	134-1501	
12.	.00	0.100	0.0030	0.9962	0.0167	0.1838	2.0770	0.8403	171.5073	

FLOW	DIA.	MANN.	SUPPLY	DEATN	DRAIN FLOH	EnTRY	NURMAL	PIPE LENGTH TO	
L/S.	M.	COSFF	SLOPE	SLUPE	ENTRY DEPTH		DEPTH	NORMAL DEPTH.	
L/30	V1.0	CGEIT	(SIN)	(SIN)	RATIO H/U.	rl _o	H/0.	L/0.	
			(3211)	431117	MAILU III U	100	117 00	2700	
								·	
	~		. 350	0 (126	0.00:0	0 25//	0 34 30	10 1 33	
		0.0090			0.0908	0.2566	0.2478	59.4608	
		0.7770			0.1422	0.4174	0.4050.	94.3054	
		0.7010			6.1864	0.5467	0.5403	121.5631	
		0.0010			U.2267	0.0075	0.6841	141.6911	
		0. 1010			0.2644	0.7555	. 0.8149	156.9853	
12.00	0.100	0.0090	0.2560	0.0125	0.3005	0.3425	0.9433	. 164.8335	
				•			•		
2 22			ř.	0 - 1 2 -		0 3: 20	2.70	(2 (122	
		0.0090			0.0737	0.3830	0.2478	62.6177	
		0.0070			0.1148	0.0302	0.4050	97.7113	
		0.0010			0.1445	0.4355	0.5483	120.9154	
		0.1010	-		0.1813	1.0108	0.6841	150.9735	
		0.0010			0.210	1.1079	0.8149	167.5933	
12.00	0.100	0.0010	0.5000	C. 0125	0.2354	1.3099	0.9438	182.0333	-
2 00			. 3.53		2 24 2	A . 34 A	2.2420		
		0.0090			0.0660	0.4749	0.2478	64-0026	
		0.7070			0.1026	0.7849	0.4050	102.0411	
		0.0340			0.1334	1.0441	0.5463	130.7371	
		0.7370			0.1615	1.2565	0.6841	151.6551	
		0.7010			0.1874	1.4704	0.8149	170.2452	
12.03	0.100	0.0010	3.7676	0.0125	0.2120	1.5537	U.9438	195.3250	
2 00	0.166	0.000		6 (12)	0.04.20	0.5337	0.2436		
		0.0070			0.0620	0.5374	0.2478	64.6025	
		0.7075			0.0961	0.3921	0.4050	107.1075	
		0.0000			0.1249	1.1691	0.5483	130-4212	
		0.3030			0.1510	1.4457	0.5041	150.5441	
		0.2330			0.1752	1.0735	0.8149	104.5000	
12.00	0.100	0.0000	0.5660	0.0125	0.1979	1.5942	0.943.5	202.4943	
2.00	0-100	0.0090	A CAFL	6 - 62 25	0.0596	0.5752	0.2478	64.3235	
		0.3033			0.0928	0.9555	0.4050	107.3534	
		0.0090			U.12U5	1.2743	0.5403	130.1474	
		0.0040			U-1450	1.2026	0.5465	149.4543	
		0.3333			0.1036	1.0052	0.5149	100.0007	
		0.00+0			0.1305	2.0352	0.9453	200.0373	
	00100	0817571	98 7C 27	0 0 0 12 7	0.1703	2 4 0 3 7 2	9.7733	20010373	
2.00	0.100	0.3090	0.5562	Cau125	Ŭ•05∀ 3	0.5658	0.2478	64.2571	
		0.0070			0.0914	0.4757	0.4050	110.7157	
		0.0000			0.1173	1.3006	0.5453	130.0000	
		0.7010			0.1442	1.0039	U. 0541	149.79.0	
		6.3010			t.1671	1419	0.6149	10001007	
		0.3030			0.1330	2.0770	0.9438	207.0 - 3	
				00117	00200		00,130		

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FLOW L/S.	DIA.	HANN. COEFF	(ZIM) ZF(:bE ZNbbFA	- •	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPTH L/D.
								·
2.00	0.100	0.0120	0.2588	0.0900	0.1092	0.1819	0.1879	23.6006
			0.2588		0.1722	0.2921	0.3030	38.9358
			0.2588		0.2267	0.3797	0-4050	50.6773
			0.2586		0.2766	0.4540	0.5015	61.3337
			0.2566		0.3235	0.5194	0.5942	70.6521
12.00	0-100	0.9120	0.2568	0.0500	3 0.3689	0.57.62	0.6841	78.2437
2.00	0.100	0.0120	0.5000	C.0500	0.0854	0.2695	0.1879	26. 2454
			0.5COC		0.1385	0.4387	0.3030	43.3731
			0.5000		0.1813	0.5765	0.4350	56.5109
			0.5000		0.2203	0.6939	0.5015	68.3543
		-	0.5000		0.2566	0.7998	0.5942	78.8214
12.00	0.100	0.3123	0.5000	0.6500	0.2917	0.8915	0.6341	87.3712
2.00	0.100	0.9120	0.7676	0.0500	0.0792	0.3332	v-1879	27.3009
4.00	0.100	0.0120	0.7070	0.0500	0.1237	0.5457	0.3030	45.1449
6.00	0.100	0.0120	0.7070	0.0500	0.1615	0.7196	0.4050	50.8053
			0.7070		0.1957	0.8715	0.5015	71.3121
			0.707C		6.2279	1.0041	0.5942	82.1718
12.00	0.100	0.3120	0.7070	0.0500	0.2585	1.1235	0.6841	91.1901
2.00	0-100	0.0120	0.8660	0.0500	0.0743	0.3769	0.1879	27.8400
			0.6660			0.0199	0.3030	46.0473
			0.8660		0.1510	0.8198	0.4050	60.1146
6.00	0.100	0.3123	0.8+60	0.0500	0.1627	0.9951	0.5015	72.8201
			0.866.0		0.2125	1.1497	0.5442	83.9447
12.00	G.1 GC	6.0120	0.8660	0.0500	0. 2498	1.2894	0.6841	93.2107
2.00	0.100	0.0120	0.9659	0.0500	C.0717	0.4036	0.1879	26.1133
			0.9659		0.111t	0.0641	0.3030	40.0043
			0.9659		G.1456	0.0797	0.4050	60.7357
8.00	0.100	0.0120	0.9659	0.0500	U.1761	1.0689	0.5015	73.5614
19.00	0.100	0. 3120	0.9654	0.0500	0.2050	1.2335	0.5942	· 84.8113
12.00	0.100	0.0120	0.9659	0.(500	0.2321	1.3662	0.6841	94.2115
2.00	0.100	0.0120	0.9962	C. 0500	0.0710	0.4117	0.1879	28.1907
			0.9962		0.1107	0.6771	0.3030	40.6272
			0.4962		0.1442	0.0973	0.4050	60.7042
8.00	0.100	0.3123	0.9962	C. 0500	0.1744	1.0894	0.5015	73.7730
			0.4962		0.2028	1.2500	0.5942	85.0633
12.00	C.100	0.0120	0.9962	0.6500	Ú.229b	1.4150	0.6641	94.4071

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2. 4. 5. 10. 12.

2. 4. 6. 3. 10.

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FLOW	DIA.	MANN.	SUFPLY	DEAIN	DRAIN FLOW	ENTRY	NURMAL	PIPL LENGTH TO
L/S.	. No	CHEFF		SLUPE	ENTRY DEPTH		DEPTH	NORMAL JEPTH.
6,30	. 114	6.7.2.1	(SIN)		RATIO H/D		H/D.	L/D.
	•		12141	(27:4)	KATIU NIU.	Пе	n/ U•	L/0-
			0 3550	0.01/3	0 1003	0 .430	0 3727	2 . 24 . 4
				0.0167	0.1092	0.1819	0.2737	32.8456
		0.0120			0.1722	0-29-21	0.4500	50.8930
6.00	0.100	0.0120	0.2586	0.0167	U. 2267	0.3797	0.6108	63.3500
5.00	Galuc	0. 3120	0.7466	0.0167	U.2756	0.4540	3.7651	72.5126
		0.0120			0.3235	0.5194	0.9146	75. 5055
		0.0120				0.2762	1.0000	70.5504
12.00	0.100	0.7120	0.2500	C.OTU.	0.3004	0.5762	1.0000	70.5554
							•	
2.00	0.100	0.0120	0.5000	0.6167	0.0084	0.2695	0.2737	35.0275
		0.0120				0.4387	0.4500	54.6024
		0.3120				0.5765	U-61U8	60.3731
		0.3120				0.6439	J.7651	70.6076
		0.3120			6.2566	0.7498	0.9146	85.3197
12.00	0.100	0.0120	0.5000	(.0157	0.2917	0.6915	1.0000	78.9110
					•			
					•			
2 - 00	6.100	0.3120	0.7070	6.0167	û.0742	0.3332	0.2737	35.9455
		0.7120			0.1237	0.0457	0.4500	50.2017
		0.0123			0.1015	0.7195	0.6108	70.6233
		0.0120				0.0715	0.7651	84.47)3
10.00	0.100	0.3123	0.7070	6.0157	U-2274	1.0041	0.9146	77.5573
12.00	0.100	0.0120	9.7070	0.0167	U.2555	1.1235	1.0000	82.7310
2 00	0.100	0 0110	0 6116	6 (1/7	. 27/2	0 2740	1 7727	3/ 50.3
		0.0120			u. 0743	0.3769	0.2737	36.5011
		0.0120			0.1155	0.5199	0.4500	57.1359 .
		0.0120			U-1510	0.0143	0.6108	72.3390
0.00	0.100	0.7120	,0.8666	0.0167	0.1527	0.9951	3.7651	80.4325
10.00	(.100	0.0120	3.8660	0.0157	0.2125	1.1447	0.4146	29.2300
		0.7120			0.2408	1.2594	1.0000	. 64.5131
2 00	0.360	0.0130	0.0445	0 (147	0.07:7	0 6.33=		2 7 7 7 7
		0.0120			0.0717	0.403b	0.2737	30.7647
		0.0120			0.1118	0.0541	0.4500	50.2225
		0.0120			0.1450		0.6108	73.0122
8,00	C-100	0.1120	0. 96.59	0.0167	0.1701	1.0084	U.7651	79.5193
10.00	C.100	0.0120	0.9659	C.0167	0.2050	1.2336	J. 7146	5.2/32
		0. 1123			0.2321	1.3862	1.0000	050.1575
2 00	0 14.0	6. 21.22	0.5010	6 (1)	. A 0712	0 (113	0 33 3	3
					0.0710	0.4117	0.2737	30.0311
		0.0120			0.1107	0.6771	0.4500	50.7452
				0.0167	0.1442	0.3973	U. 6100	74.2157
5.00	0.100	0.0120	0.490.2	0.(167	0.1744	1.0594	0.7601	74.4007
10.00	0.100	0.0120	0.4962	C. L167		1.2500	0.9146	-4.7103
		U. 3129				1.4150	1.0000	86.1437
	(0 2 0 0	00 74 2 7	00 9 90.2	0.00101	0 6 2 2 7 10	10 12 70	1.0000	0002137

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103.5747

0.2949

12.00 0.100 0.0120 0.9962 0.0250 0.2246

	/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIN)	DEAIN SLUPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/G.	ENTRY ENERGY	NORMAL DEPTH H/D.	PIPE LENGTH TO NORMAL JEPTH. L/D.
								٠.	·
		15							
				0.2588		0.1092	0.1819	0.3030	32.6191
N				0.2566		0.1722	0.2921	0.5015	44.0051
Ш				0.2588		0-2267	0.3797	0.6841	50.8049
١,				0.2558		0.2766 0.3232	0.4540	1.0000	64.1542 65.0564
				0.2588		0.3689	0.5762	1.0000	59.3667
ľ	2.00	0.100	0.117.2	0.2.00		0.3007	0.5702	1.000	3743007
П				ň					
	2.00	0.100	0.0120	0.5000	0.0125	0.0384	0.2695	030 هدن	34.8062
	4,119	0.100	0.0120	0.5000	0.0125	0.1385	0.4387	0.5015	52.7402
	6.10	0.100	0.0120	0.5000	0.0125	U. 1313	0.5765	0.6841	63.87.13
				0.5000		0.2203	0.6939	0.8509	70.4113
				0.5000		0.2506	0.7995	1.0000	72.3524
]	12.00	G-100	0.0120	0.5000	C.C125	0.2917	0.8915	1.0000	67.5700
ľ									
ı	2.00	6. 166	0.0123	0.7070	6 6125	0.0792	0.3332	0.3030	35.7892
				0.7070		6.1237	0.5457	0.5015	53.6059
				0.7076		0.1615	0.7196	0.6541	62.5629
				0.7070		0.1957	0.6715	0.8559	72.9033
7				0.7076		0.2279	1.0041	1.0000	75.6515
				0.7676		U.2505	1.1239	1.0000	71.3477
	_								
				0.8660		0.0743	0.3769	0.3030	30.0654
				0.000		0.1158	0.6199	0.5015	52.5119
				0.8660		0.1510	0.0198	0.6841	26.4357
,				0.8666		0.1527 0.2125	0.4951	1.0000	74.3143 77.4503
				0.8660		0.2408	1.2694	1.0000	73.4075
1	1	0.100	04 7 2 2 3	000000		002100	102071	1.0000	134 1013
				0.9659		U.0717	0.4036	0.3030	30.1100
				0.9659		0.1118		0.5015	51.4450
				0.9659			0.3797	0.5541	606 5303
				0.4659			1.0689	J. 3509	75.0045
				0.9654			1.2335	1.0000	78.3521
4	12.00	6-160	0.7120	0.5654	0.0175	0.2321	1.3862	1.0000	74.44.5
							2		
	2.00	6.160	0.0120	0.996	0.0125	ŭ.971u	0.4117	0.3030	36.1170
				0.9562		0.0710		0.5015	51.75/7
				0.9962		U.1442	0.5773	0.6341	60.9435
				0.44+2			1.0074	J. 6 7 5 9	75.1333
	10.00	0.166	0.1120	11.4466	C. U. /:		1.2000	1.0000	70.01.4
	12.00	C-10C	0.0120	0.9962	C. C125	0.22+6	1.4150	1.0000	74.73.1

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FLOW L/S.	DIA.	MANN. COEFF	SUPPLY (SIM)		DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH .H/D.	PIPE LENGTH NORMAL DEPT L/O.
2.00	0.100	0.0150	0.2 5 88	6- 0500	0.1263	0.1404	0.2184	16.0500
		0.0150			0.2001	0.2237	0.3552	27.3555
		C. 0150			0.2644	0.2889	U-4778	35.2204
		0.0150			. 0.3235	0.3441	0.5942	42.0155
		0.0150			0-3901	0.3907	0.7056	46.7747
12.00	0.166	0.0150	0.2568	0.0500	℃. 4 34 3	0.4325	0.8149.	51.1932
		0.915.0			0.1020	0.2062	0.2184	18.5129
		0.0150			0.1605	0.3325	0.3552	30.3949
		0.0150			0.2168	0.4339	0.4778	39.2359
		0.0150			0.2566 0.30u0	0.5211	0.5942 0.7056	40.8532 52.3797
		0.0150			0.3420	0.0616	0.8149	57.4165
12.00	7.00	0.3170	0.000	0.03.90	0.3420	0.0010	0.0117	716 420 3
		G. 0150			0.0912	0.2540	0.2154	19.2531
		0.0150			0.1432	0.4121	0.3552	31.5737
		0.0150			0.1874 0.2279	0.5413	0.4778 0.5942	40.4653 48.9375
		0.0150			0.2659	0.7476	0.7056	54.0147
		0.7150			0.3020	0.8349	0.8149	60.2076
		0.0150			0.0855	0.2374	0.2184	19.6637
		0.0150				0.4682	0.35./2	32.3454
		0.0150			0.1752	0.6155	0.4770	41.3573 50.0500
		0.7150			0.2125 0.2478	0.7435 0.8546	0.5942	56.1120
		0.3150			0.2515	0.9544	0.8149	61.6505
		0.0150			0.0326	0.3072	0.2104	19.8852
		0.0150			0.1293	0.5009	0.3552	32.0777
		0.0150			0.1658	0.0607	0.4778	42.3201
		0.0150			0.2050	0.7970	0.5942 0.7056	50.5975 5c.7715
		0.0150	-		0 • 2356 0 • 2708	0.7189	0.7058	62.4205
12.00	00100	0.3133	0.7037	(0 0 0 0 0	0.2100		003217	02.1203
		0.0150			0.0318	0.3125	0.2184	19.9352
		0.0150			0.1278	0.5120	0.3552	32.7547
		0.0150			0.1671	0.0737	0.4778	42.4444
		0.0150			0.2028	0.0137	0.5942 0.7056	50.75=2 56.9430
		0.0150			0.2352 0.2578	1.0500	0.5149	62.6275
12.00	0.100	0.0100	30 7702	C & U) () U	0.2310	22000	0.0177	02.0277

1548	L/S.	DIA.	MANN. COEFF	SUPPLY SLCPE (SIN)	DPAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENERGY	NORMAL DEPTH H/D.	PIPE LENGTH TO NORMAL DEPTH. L/D.
	4.00 6.00 8.00 10.00	0.160 0.166 0.166 0.166	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.2560 0.2560 0.2568 0.2588	0.0250 0.0250 0.0250 0.0250	0.1263 0.2001 0.2644 0.3235 0.3501 0.4343	0.1404 0.2237 0.2659 0.3441 0.3907 0.4325	0.2776 0.4573 0.6216 0.7778 0.9302 1.0000	19.8050 30.7053 30.0392 42.7503 45.3750 39.4603
	4.00 6.00 8.00	0.160 0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.5000 0.5000 0.5000 0.5000	0.0250 0.0250 0.0250 C.0250	0.1020 0.1605 0.2108 0.2506 0.3300 0.3420	0.2062 0.3325 0.4339 0.5211 0.5961 0.6516	0.2776 0.4573 0.6216 0.7778 0.9302 1.0000	21.4309 33.4152 41.6651 47.1850 51.0515 45.3349
	4.00 6.00 8.00 10.00	0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.7070 0.7070 0.7070 0.7070	0.0250 0.0250 0.0250 0.0250	0.0912 0.1432 0.1874 0.2279 0.2659 0.3020	0.2540 0.4121 0.5413 0.650° 0.7476 0.8349	0.2776 0.4573 0.6216 0.7776 0.9302 1.0000	22.1506 34.6397 43.3302 49.2103 53.4375 4c.1274
	4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0150 6.7150 6.0150 0.0150 6.0150 0.0150	0.8660 0.8660 0.8660	0.0250 0.0250 0.0250 0.0250	0.0355 0.1339 0.1752 0.2125 0.2475 0.2315	0.2874 0.4662 0.0155 0.7435 0.8540 0.9544	0.2776 0.4573 0.6216 0.7778 0.9302 1.0000	22.5422 35.3003 44.2111 50.3236 54.7350 49.6075
	4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.9659 0.9659 0.9659 0.9659	0.0250 0.0250 0.0250 0.0250	0.0326 0.1293 0.1658 0.2050 0.2386 0.2758	0.3072- 0.009 0.6607 0.7470 0.9133 1.0283	0.2776 0.4573 0.6216 0.7778 0.9302 1.0000	24.7390 35.6314 44.5724 50.3313 55.4007 50.3952
	4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	C.0150 G.0150 G.0150 G.0150 G.0150	0.9962 0.9962 0.9962 0.9962	0.0250 0.0250 0.0250 0.0250	0.127s 0.1671 0.201s	0.3125 0.5120 0.5737 0.5137 0.7371 1.0500	0.2776 0.4573 0.6216 0.777c 0.93u2 1.0000	22.7051 35.7361 44.7733 51.0423 55.5795 50.6114

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIN)	SLOPE	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORHAL DEPTH H/D.	PIPE LENGTH NORMAL DEPI L/D.
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.2566 0.2566 0.2508 0.2586	0.0167 0.0167 0.0167 0.0167	0.1263 0.2001 0.2644 0.3235 0.3801 0.4343	0.1404 0.2237 0.2869 0.3441 0.3907 0.4325	0.3201 0.5317 0.7271 0.9170 1.0000	16.9767 27.4700 31.2717 31.3953 34.2745 32.0298
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.5000 0.5000 0.5000 0.5000	0.0167 0.0167 0.0167 0.0167	0.1020 0.1505 0.2100 0.2566 0.3000 0.3420	0.2062 0.3325 0.4339 0.5211 0.5961 0.6616	0.3201 0.5317 0.7271 0.9146 1.0000	20.5906 30.1562 34.9049 34.7729 39.3945 37.7511
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150 0.0150	0.7076 0.7076 0.7076 0.7076	0.0167 0.0167 0.0167 0.0167	0.0912 0.1432 0.1874 0.2279 0.2659 0.3020	0.2540 0.4121 0.5413 0.0503 0.7476 0.3349	0.3201 0.5317 0.7271 0.9146 1.0000 1.0000	21.3256 31.4352 30.6021 35.7424 41.7854 40.4953
4.00 6.00 8.00 10.00	0.100 0.100 0.100 0.160	0.0150 0.0150 0.0150 0.0150 0.0150	0.8660 0.8660 0.8660 0.8660	0.0167 0.0167 0.0167 0.0167	0.0855 0.1339 0.1752 0.2125 0.2478 0.2815	0.2874 0.4682 0.6155 0.7435 0.0548 0.7544	0.3201 0.5317 0.7271 0.9146 1.0000 1.0000	21.7209 32.1797 37.5057 35.7791 43.0914 41.9543
4.00 6.00 8.00 10.00	0.100 6.100 0.100 0.100	0.0150 0.0150 0.0150 0.0150 0.0150	0.9659 0.9659 0.9659 0.9659	0.0157 0.0157 0.0157 0.0157	0.0326 0.1293 0.1608 0.2050 0.2386 0.2708	0.3072 0.5009 0.6607 0.7970 0.9183 1.0283	0.3201 0.5317 0.7271 0.9146 1.0000	21.9229 32.8039 37.9801 35.4811 43.7029 42.7326
4.00 6.00 8.00 10.00	C.1CO O.1CO C.1UC O.1OO	0.0150 0.0150 0.0150 0.0150 0.0150	0.9962 0.9962 0.9962 0.9962	0.0167 0.0167 0.0167 C.0167	0.0318 0.1278 0.1671 0.2028 0.2362 0.2578	0.3125 0.0120 0.0737 0.d137 0.9371 1.0000	0.3201 0.5317 0.7271 0.9146 1.0000	21.9733 33.0017 36.1032 35.3344 43.9433 42.9462

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12. 6. 10.

8.0 6.0 10.0 12.0

841	LOH /S.	DIA.	MANN. COEFF	SUPPLY SLGPE (SIN)	DRAIN SLLPE (SIN)	DRAIN FI DRAINS OH CITAS	EPTH EMERGY	NURMAL DEPTH H/D.	PIPE LENGTH TO NOKHÁL JEPTH. L/D.
100 mm m m m									
ì	2 00	0 160	6 01=0	0.2606	0 0136	0.137	2 0 1404	A 2652	16 4147
				0.2586		0.126		0.3552 0.5942	15.8132 16.2155
				0.2588		0.2644		0.8149	
				0.2585		0.323		1.0000	24.9474
				0-2566		0.330		1.0000	30.7114
				0.2566		0.434		1.0000	24.5873
Ī									
П									
				0.5100		0-1020		0.3552	17.3246
					0.0125	0.160		0.5942	23.2361
				0.5000		0.2108		0.8149	20.7443
				0.5000		0.256		1.0000	26.7235
				0.5660		0.300		1.0000	35.7013
1	2.00	0.100	C.0150	0.5000	0.0125	0.342	0.0016	1.0000	35.3444
							•		
	2 00	0 160	6 0150	0.7070	0 0135	0.091	2 0.2540	0.3552	16.0009
				0.7070		0.143		0.5942	23.7755
				0.7070		0.137		0.3742	24.5054
				0.7070		0.227		1.0000	20.5257
				0.7676		U . 265		1.0000	30.1557
				0.7070		0.302		1.0000	30.0076
Ĭ					••••	00302			3000070
	2.00	G.1CC	0.0150	0.8660	C.0125	0.095	5 0.2874	0.3552	10.3505
	4.00	0.100	0.0150	0.8660	0.0125	0.133	9 0.4682	0.5942	24.1323
				0.8666		C.175		0.8149	24.0623
				0.8660		0.212		1.0000	29.53.3
				0.6660		0.247		1.0000	34.4547
1	2.00	0.100	0.0150	0.6666	0.6125	0.281	0.4544	1.0000	39.5213
	2 00	0 100	0 2152	0.9659	0 (126	(: 0.43)		0 2552	1 = 50=2
				0.9659		0.002		0.3552 0.5942	10.53±3 24.31±0
				0.9659		U • 100		0.8149	24.0021
			-	0.7659		0.205		1.0000	30.0373
				0.9659		0.205		1.0000	40.123)
				0.9659		0.270		1.0000	40.2420
			, ,			5.2. 0	200003	2 0 0 0 0	1002/70
	2.00	0.100	0.0150	0.9962	0.0125	0.001	0.3125	0.3552	10.5535
	4.00	C.luc	6.7120	0.4962	C. C125	0.127		0.5942	24.3757
				0.9962		0.167		0.8149	24.3417
				0.4962		0.202		1.0000	36.1552
				0.6965		0.230		1.0000	40.57.3
1	2.00	0.100	0.7150	0.9962	C. C125	0.201	d 1.500	1.0000	40.5033

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FLOW	DIA.	MANN. COEFF	SUPPLY SLOPE (SIN)	SLOPE	DRAIN FLOW ENTRY DEPTH RATIO H/D	ENTRY . ENERGY M.	NORMAL DEPTH M/D.	PIPE LENGT: NORMAL DEP L/D.
					•			
			0.2588		0.1422	0.1150	0.2478	12.3656
			0.2560		0.2207	0.1814	0.4050	14-4377
			0.2558		0.3005 0.3689	0.2332	0.5453	24.9289 20.8658
			0.2500		0.4343	0.3136	0.8149	31.5926
12.00	0.100	0.0110	0.2588	0.0500	0.4976	0.3462	0.9438	33.8857
2.00	0.100	0.0130	0.5000	0.0500	0.1143	0.1662	0.2475	13.7195
			0.5000		0.1813	0.2663	0.4050	21.6457
			0.5000		0.2369	0.3454	0.5433	27.8114
			0.5000		0.2917	0.4124	0.6841	32.3343
			0.5000		0.3420 0.3849	0.4699	0.8149	35.5683 38.3230
22800	04200	0.7230		0.80900			067130	3047230
2.00	0.100	0.0130	0.7070	0.0500	0.1026	0.2039	0.2478	14.3051
			0.7070		0.1615	0.3288	0.4050	22.5220
			0.7070		0.2120	0.4293	0-5483	24.1253
			0.7670		0.2565 0.3020	0.5138	J.6841 J.6149	33.9152 37.4319 I
			0.7070		0.3440	0.6546	0.9438	40.4007
2.00	0.100	0.0130	0.8666	0.0500	0.0961	0.2302	0.2478	14.6122
			0.8666		0.1510	0.3728	0.4050	23.1413
			0.8666		0.1979	0.4884	0.5403	24.8225
			0.8660		0.2438 0.2315	0.5664	0.6841	34.7701 30.4170
			0.6660		0.2313	0.7484	0.943 d	41.5232
2.00	0.100	0.0130	0.9659	C. C50.0	0.0928	0.2458	0.2478	14.7077
			0.9659		0.1456	0.3991	U.4050	23.4078
			0.9659		0.1908	075231	0.5453	30.1730
			0.9654		0.2321 0.270c	0.0290	0.6841	35.2075 30.9355
			0.4659		0.3079	0.5052	0.9438	42.1059
				0.6500		0.2508	0.2478	14.2130
			0.9962		0.1442	0.4068	0.40>0 0.5483	23.4804
			0.9962		U.1308 U.2296	0.5334	0.5483	35.3230
			0.9962		0.2675	0.7374	0.8149	34.0773
12.00	0.100	0.7130	0.4962	0.0500	0.3044	0.3223	0.9438	42.2790

2. 4. 6. 10.

2. 4. 6. 8. 10.

2. 4. 5. 8. 17.

10	\2.	DIA.		SUPPLY SLOPE (SIM)	SLEPE	DRAIN FLOW ENTRY DEPTH RATIO H/D.		NORMAL DEPTH H/D.	PIPE LENGTH TE NORMAL DEPTH. L/D.
1	4.00 6.00 9.00 0.00	G.166 0.100 G.160	0.0130 0.0130 0.0130 0.0130	0.2568 0.2568 0.2568 0.2568 0.2568	C.C250 C.0250 O.C250 O.C250	0.1422 0.2207 0.3005 0.3659 30.4343 0.4976	0.1150 0.1:14 0.2332 0.2766 0.3135 0.3462	0.3157 0.5239 0.7153 0.8949 1.0000	12.6444 18.3104 21.0327 22.7092 22.2029 20.1535
1	4.00 6.00 8.00 0.00	0.100 0.100 0.100 0.100	0.9189 0.0199 0.0139 0.0130	0.5000 0.5000 0.5000 0.5000 0.5000	0.0250 0.0250 0.0250 0.0250	0.1148 0.1813 0.2359 0.2917 0.3429 0.3599	0.1662 0.2663 0.3454 0.4124 0.4699 0.5218	0.3157 0.5239 0.7103 0.5999 1.0000 1.0000	13.8540 20.3515 23.7553 25.1934 25.9423 24.3777
1	4.00 6.00 8.00 0.00	f.100 6.100 6.100 6.100	0.0130 0.0130 0.0140 C.0140	0.7070 0.7070 0.7070 0.7070 0.7070	0.0250 0.0250 0.0250 0.0250	0.1026 0.1515 0.2120 0.2585 0.3020 0.3440	0.2039 0.3229 0.4293 0.5139 0.5890 0.6546	0.3157 0.5239 0.7163 0.3999 1.0000	14.4224 21.3103 25.0505 26.6153 27.77:1 26.4252
1	4.00 6.00 6.00	C.166 C.160 C.166	0.0130 0.0130 0.0130 0.0130	0.8660 0.7660 0.7660 0.8660	0.0250 0.0250 0.0250 0.0250	0.0961 0.1510 0.1979 0.2406 0.2615 0.3201	0.2302 0.3723 0.4684 0.5664 0.0714 0.7484	0.3157 0.5239 0.7163 0.5949 1.0000	14.7230 21.3322 25.7719 27.4109 28.7690 27.5532
1	4.00 6.00 5.00 0.00	C.166 C.166 C.166	0.0130 0.0130 0.0130 0.0130	0.9659 0.9659 0.9659 0.9659	0.0750 0.0750 0.0250 0.0250	0.0928 0.1456 0.1906 0.2321 0.2705 0.3079	0.2458 0.3991 0.5231 0.6290 0.7224 0.6052	0.3157 0.5239 0.7163 0.8999 1.0030	14.3545 22.1017 26.1328 27.3233 24.2717 20.1413
1	4.00 5.00 8.00 0.00	0.100 0.100 0.100 0.100	0.0130	0.9962 0.9962 0.9962 0.9962 0.9962	0.0250 0.0250 0.0250 0.0250	0.0919 0.1442 0.1338 0.2296 0.2673 0.3044	0.2503 0.4063 0.5334 0.5417 0.7374 0.0223	0.3157 0.5239 0.7163 0.8999 1.0000	14.9307 24.1757 20.2323 27.7372 24.4300 20.3373

FLOW L/S.	DIA. MANN. N. CDEFF	SUPPLY DEAL STOP	E ENTRY DEPTH	ENTRY ENERGY M.	NORMAL DEPTH H/D•	PIPE LENGTH MORMAL DEPTH L/D.
4.00 6.00	0.100 0.013	0 0.2588 0.01 0 0.2588 0.01 0 0.2566 0.01	67 0.2267 67 0.3005	0.1150 0.1514 0.2332	0.3645 0.6108 0.8403	9.3670 12.1475 6.3572
10.00	0.100 0.011	0.2588 0.01 0.2588 0.01 0.2588 0.01	67 0.4343	0.2766 0.3136 0.3462	1.0000	14.0193 15.8451 10.0135
4.00 6.00 8.00 10.00	0.100 0.0130 C.100 0.0130 G.100 0.0130 G.100 0.0139	0 0.5000 0.01 0 0.5000 0.01 0 0.5000 0.01 0 0.5000 0.01 0 0.5000 0.01	67 0.1813 67 0.2369 67 0.2917 67 0.3420	0.1662 0.2663 0.3454 0.4124 0.4649	0.3645 0.6108 0.8403 1.0000	10.4300 13.1223 11.6095 17.8543 22.5134
2.00	C.100 0.0130	0.5000 (.C1 0.7070 0.C1 0.7070 0.C1 0.7070 0.C1	67 0.1026 67 0.1615	0.5218 0.2039 0.3258 0.4293	0.3645 0.6108 0.8403	22.11d5 10.9101 13.7955 12.1033
8.00 10.00	0.100 0.0130	0.7070 0.01 0.7070 0.01 0.7070 0.01	67 0.25 85 67 0.3 020	0.5138 0.5890 0.6545	1.0000	19.3149 24.3290 24.1419
4.00 6.00 8.00 10.00	0.100 0.0130 0.100 0.0130 0.100 0.0130 0.100 0.0130	0 0.8660 0.01 0 0.8660 0.01 0 0.8660 0.01 0 0.66.0 0.01 0 0.8660 0.01	67 0.1510 67 0.1979 67 0.2406 57 0.2515	0.2302 0.3728 0.4884 0.5864 0.5714 0.7484	0.3645 0.6106 0.8403 1.0000 1.0000	11.1576 14.1373 13.2420 20.1375 25.3057 25.2554
4.00 6.00 8.00 10.00	0.100 0.0130 C.100 0.0130 0.100 0.0130 G.100 0.0130	0 0.9659 0.01 0 0.9659 0.01 0 0.9659 0.01 0 0.9659 0.01 0 0.9659 0.01	67 0.1456 67 0.1908 67 0.2321 67 0.2708	0.2458 0.3991 0.5231 0.6290 0.7224 0.8052	0.3645 0.6106 0.8403 1.0000 1.0000	11.2304 14.3042 13.3073 20.5572 25.8293 25.8332
4.00 6.00 8.00 10.00	0.100 0.0130 0.100 0.0130 0.100 0.0130 0.100 0.0130	0 0.9962 C.01 0 0.9962 C.01 0 0.9962 C.01 0 0.9962 C.01 0 0.9962 C.01	67 0.1442 67 0.1888 67 0.2276 57 0.2578	0.2508 0.4068 0.5334 0.5417 0.7374	0.3645 0.6108 0.8403 1.0000 1.0000	11.3101 14.3407 13.3975 20.6752 25.9741 26.0027

D = 0.15

						•		
FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIN)	CRAIN SLOPF (SIN)	DRAIN FLOH ENTRY DEPTH RATIO H/C.	ENTRY ENERGY M.	MORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPT L/D.
							-	
							<u>.</u> 4,	
	4							
		0.0090			0.0460	0.1973	0.0770	17.4232
		0.0030			0.0710 0.0919	0.3303 0.4433	0.1201	29.7004 41.1016
		0.0070	-		0.1104	0.5451	0.1901	50.8775
		0.0090			0.1278	0.0355	0.2211	54.6272
12.00	0.150	0.3390	0.2588	0.0500	0.1439	0.7215	0.2507	60.5173
			r.					
		0.0090			0.0375	0.2919	0.0770	14.4553
		0.0090			0.0577	0.4924	0.1201	33.3104
	-	0.00+0			0.0744 0.0594	0.6659 0.c193	0.1569 0.1901	46.0027 50.7811
		0.3090			0.1032	0.7005	0.2211	66.6033
		0.0090			0.1160	1.0943	0.2507	70.4602
						•		
2.00	0.150	0.0090	0.7070	C.0500	0.0337	0.3592	0.0770	20.2637
		0.0090			0.0518	0.0084	0.1201	34.6491
		0.0090			0.0667	0.5244	0.1569	47.8109
		0.0070			0.0400	1.0184	0.1901	59.0542 69.2551
		0.7070			0.0923 0.1038	1.3606	0.2507	79.5004
~ ~ ~ ~ ~ ~	00230		00,000			243000	002301	
2.00	0.15C	0.0090	0.8666	C.U500	0.0316	0.4069	0.0770	20.6519
		0.3330			U. 0480	0.6589	0.1201	35.3224
		0.0070			0.0526	0.9354	0.1569	48.7233
		0.0000			0.0751 0.0865	1.1527	0.1901	60.1559 70.6539
		6.0030			0.0372	1.5482	0.2507	81.0546
12.00	00230		000.000	(• 0) 0 0	0.0712	107102	0 1 2 3 0 1	01007.0
2.00	0.150	0.0070	0.9659	0.0500	0.0306	0.4344	9.0770	20.3545
4.00	0.150	0.0070	0.9659	0.0400	0.0470	0.7373	0.1201	35.6512
		0.0090			0.0605	0.7988	0.1509	44.1602
		0.2010			0.0726	1.2344	0.1901	60.7381
		0.0090			0.0336 0.0938	1.4545	0.2211 0.25J7	71.3195 81.3403
12.00	60196	0 6 9 9 7 0	0.9029	0.0000	0.0730	140014		V 2 4 0 1 C J
2.00	0.150	0.0090	0.9962	C. 05 30	0.0303	0.4426	0.0770	20.9075
		0.0090			0.0455	0.7507	0.1201	35.7451
		0.0070			0.0599	1.0189	0.1509	44.2954
		0.0070			0.0710	1.2593	0.1901	60.3957
		0.0010			0.0827 0.0930	1.4644	0.2211 0.2507	71.5117 82.0347
12.00	C. 130	0.0070	0.7702	1.0000	0.0430	1.0411	0.2701	02.00341

							•			
ı	FLCH	DIA.	MANN.	SUFPLY	CRATH	DRAIN FLOW	ENTRY	NURMAL	PIPE LENGTH TO	
			COEFF	SLCPE	SLUPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPTH.	
	L/S.	M.	LUEFF							
				(ZIM)	(214)	RATIO H/D.	M.	H/D.	L/U.	
			•							
Н							0.000			
				0.2586		0.0460	0.1973	0.0960	24.4377	
	4.00	0.150	0.1070	0.2588	0.0250	0.0710	0.3303	0.1508	41.7575	
	6.00	G.150	0.7030	0.2566	0.0250	0.0919	0.4433	0.1976	50.3043	
	5.00	0.150	0-2070	0.2568	0.1250	0.1104	0.5451	0.2436	67.0375	
				0.2580		U.1275	0.0355	0.2810	81.7440	
				0.2568		0.1439	0.7215	0.3196	92. 3807	
	12.00	0.100	0.5770	702300	0.02.15	0.1137	00.617	0.3170	, e e , 50 ,	
					•			•		
				i i						
	2.00	0.150	0.0090	0.5000	C+0250	0.0375	0.2919	0.0950	26.1320	
	4.00	0.150	0.0090	0.5000	0.0250	0.0577	0.4924	0.1508	44.0034	
	6.00	C.15C	0.7070	0.5000	0.0250	0.0744	0.6659	J.1976	60.2949	
				0.5000		0.0894	0.0193	0.2406	74.5432	
				0.5000		0.1032	0.4600	0.2510	67.0155	
							1.0943	0.3146	94.5453	
	12.00	0.150	C • 20 4 7	0.5000	0.0270	0.1160	1.0943	0.3140	77.5453	
	2.00	0.150	0.0030	0.7070	0.0250	0.0337	0.3592	0.0960	26.3259	
	4.00	0.150	0.9990	0.7070	0.0250	0.0510	0.0084	0.1508	45.3012	
				0.7076		U.06.7	0.0244	0.1976	61.9342	
				0.7070		0.0800	1.0184	0.2406	70.6537	
				0.7676		0.0723	1.1944	0.2310	90.6452	
	12.00	0.150	0.0030	9.7C7L	0.0250	0.1035	1.3605	0.3196	102.3113	
	2.00	0.150	0.0000	0.0660	0.0250	U.031c	0.4069	0.0900	27.1915	
	4.00	0.150	0. 70 10	2.8460	0.0250	0.0436	0.5089	0.1508	40.4305	
				0.8660		U. 0620	0.9354	0.1976	62.7912	
				0.16.3		0.0751	1.1527	0.2406	77.6935	
				0.8666		0.0365	1.3589	0.2510	91.3214	
	12.00	0.150	0.3040	0.8660	0.0250	0.0472	1.5482	0.3196	103.7594	
	2.00	0.150	0.0000	0.4654	C. (250	6.0360	0.4344	0.0960	27.37.7	
	4.00	0.150	0. 77.40	0.9659	0.0250	0.0470	0.7373	0.1508	40.7 101	
	6.00	0.150	0.0000	0.9659	0.6250	0.0605	0.9988	0.1476	63.2053	
				0.56.59		0.0726	1.2344	0.2406	70.6314	
				0.9659		U • 0 # 3 c	1.4545	0.2010	91.9413	
									= :	
	12.00	(.150	0.7790	0.9659	0.0.750	0.0938	1.0014	3.3146	104.5153	
				0.9962		0.0303	0.4426	0.0960	27.42.2	
	4.00	0.150	0.1070	0.4962	0.6251	.0.0405	0.7507	0.1508	40.3775	
	6.00	0.150	6.7310	0.9962	0.0250	0.0549	1.0189	U. 1976	03.3237	
				0.5962		0.071	1.2593	0.2406	70.3114)	
				2.4962		0.0547	1.4644	0.2510	92.1323	
				0.5962		0.0930	1.0917	0.3146	164.7014	
	12.00	0.150	0.0.77	0.7762	(0 0 2 5 0	0.0430	1.0917	0.2140	104.7024	

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FLOW	DIA.	HANN.	SUPFLY	CRAIN	DRAIN FLOH	ENTRY	NORHAL	PIPE LENGTH 1
L/S.	M.	COEFF	SLEPE	SLOPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPTH.
	•••	•	(SIN)	(SIN)	RATIO H/D.	n.	H/D.	L/D.
			(34,11)	4 3 2 11 7	AM110 11700	***		2,0.
								8
							•	:
					•			
3 00		0.0000	0.0563	0.01/3	0.0440	0.1033	0 1003	30 3300
		0.1090			0.0460	0.1973	0.1093	28.3700
		0.0000			0.0710	0.3303	0.1725	48.0323
		0.0030			0.0919	0.4433	0.2269	05.5376
		0.0000			0.1104	0.5451	0.2766	79.5574
		0.7770			0.1278	0.6355	0.3240	93.3956
12.00	0.150	0.0010	0.2568	C.0167	10.1439	0.7215	0.3694	106.0670
_								
		0.0030			0.0375	0.2919	0.1093	29.9749
		0.0090			0.0577	0.4924	0.1725	51.3783
		0.7070			0.0744	0.6659	0.2259	69.3157
8.00	0.150	0.0070	0.5000	0.0167	0.0844	0.0193	0.2756	84.2703
10.00	0.150	0.0000	0.5000	C.0167	0.1032	0.9605	0.3240	90.9729
12.00	0.150	0.0090	0.5000	0.0167	0.1100	1.0943	0.3574	112.43++
								1112
								Y
2.00	0.150	0.0030	0.7070	C.C167	0.0337	0.3592	0.1093	30.6493
		0.0090			0.0518	0.6084	0.1725	52.5401
		0.0000			0.0667	0.6244	0.2269	70.9004
		0.0010			0.0500	1.0184	0.2766	80.2957
		0.0770			0.0923	1.1944	0.3240	101.3557
		0.0070			0.1038	1.3606	0.3694	115.1521
22.50	(12)(0.0070	5.7070	(0 0 1 0 1	0.1030	10000	0.3074	1112
								- 1
2 00	0 150	0.0070	0 8640	0.0167	0.0316	0.4069	0.1093	31.0087
		C. 3070				.0.689	0.1725	53.1465
		0.0030			0.0626	0.9354	0.2269	71.7455
						1.1527	0.2766	87.32±5
		0.0070			0.0751			103 (3:3)
		0.0090				1.3589	0.3240	102.61.49
12.00	0.150	0.0070	0.8666	0.0167	0.0972	1.5482	0.3694	110.5944
								10
3 00	0 150						0. 10.:0	21 1.51
		0.0090			0.0306	0.4344	0.1093	31.1056 53.4557
		0.0090			0.0470	0.7373	0.1725	736 4701
		0.0070			0.0605	0.4985	0.2269	4 E 0 E 7 E 0
		0.0000			0.0726	1.2344	0.2766	0163313
		0.0010			0.0836	1.4545	0.3240	103.2452
12.00	0.150	0.3340	0.9659	0.0167	0.0936	1.0614	0.3694	117.335=
								144
		0.0030		-	0.0303	0.4426	0.1093	31.2345
		0.0770			0.0465	0.7507	0.1725	53.5333
		0.0090			0.0549	1.0189	0.2269	72.2734
		0.0000			0.0710	1.2593	0.2706	85.3155
		0.0000			0.0827	1.4844	0.3240	103.4200
12.00	0.150	0.0090	0.9962	0.0167	0.0930	1.0917	0.3644	117.52.14

600	LOW ./S.	DIA.	MANN. COEFF	SUPPLY (SIN)	DRAIN SLUPE (SIN)	DRAIN FLOW ENIRY DEPTH RATIO H/D.	ENTRY ENERGY	NORMAL DEPTH H/J.	PIPE LENGTH TO NORMAL DEPTH- L/U.
	4.00 6.00 6.00 0.00	0.150 0.150 0.150 0.150	0.0090 0.0090 0.0090 0.0090 0.0090	0.2566 0.2566 0.2566 0.2566	C.6125 C.6125 C.6125 C.6125	0.0460 0.0710 0.0919 0.1104 0.1278 0.1439	0.1973 0.3303 0.4433 0.5451 0.6355 0.7215	0.1201 0.1901 0.2507 0.3064 0.3596 0.4104	30.8745 52.7255 70.8920 56.1145 100.6511 113.3210
,	4.00 6.00 8.00 0.00	0.150 0.150 0.150 0.150	0.0070 0.0070 0.0070 0.0070 0.0070 0.0070	0.5000 0.5000 0.5000	0.0125 0.0125 0.0125 0.0125	0.0375 0.0577 0.0744 0.0894 0.1032 0.1160	0.2919 0.4924 0.0059 0.0193 0.9006 1.0943	0.1201 0.1901 0.2507 0.3004 0.3596 0.4104	32.4492 55.4249 74.6103 90.7375 100.3343 119.6243
2	4.00 6.00 8.00 0.00	0.150 0.150 0.150 0.150	0.0090 0.0090 0.0090 0.0090 0.0090 0.0090	0.7670 0.7670 0.7670 0.7670	0.0125 C.0125 O.0125 C.0125	0.0510	0.3592 0.6054 0.6244 1.0184 1.1944 1.3606	0.1201 0.1901 0.2507 0.3064 0.3596 0.4104	33.12J3 56.58J3 76.1970 92.7538 106.70J3 122.3338
	4.00 6.00 3.00 10.00	0.150 0.150 0.150 0.150	0.0090 0.0090 0.0090 0.0090 0.0090	0.8660 0.8660 0.8660	C.0125 C.0125 C.0125 C.0125	0.0316 0.0456 0.0626 0.0751 0.0355 0.0972	0.4069 0.6039 0.9354 1.1527 1.3589 1.5482	0.1201 0.1901 0.2507 0.3004 0.3096 0.4104	33.4793 57.1957 76.7059 95.0953 107.0147 81.0642
	4.00 6.00 8.00 10.00	0.150 (.150 0.150 0.150	0.3070 0.3370 0.3370 0.3370 0.3370 0.3370	0.9659 0.9659 0.9659 0.9659	0.0125 0.0125 0.0125 0.0125	0.0306 0.0470 0.0605 0.0726 0.0336 0.0938	0.4344 0.7373 0.9985 1.2344 1.4545 1.5614	0.1201 0.1901 0.2507 0.3004 0.3090 0.4104	33.55.2 50.65.2 75.51.1 97.45.25 105.41.37 50.1434
	4.00 6.00 n.00	0.150 0.150 0.150 0.150	0.0090 0.0090 0.0090 0.0090	0.9962 0.4962 0.4962 0.9962	0.6125 0.6125 0.6125 0.6125	0.0303 0.0405 0.0595 0.0718 0.0327 0.0330	0.4426 0.7507 1.0189 1.2593 1.4644 1.5917	0.1201 0.1901 0.2507 0.3004 0.3770	33.7053 56.5372 75.2747 90.3451 104.7503 52.2573

FLOW	DIA.	MANN.	SUPPLY	DRAIN	DRAIN FLOW	' ENTDY	NORHAL	PIPE LENGTH T
L/S.	Me.	COEFF	SLOPE		ENTRY DEPTH	ENERGY	DEPTH	MORMAL DEPTH.
			(SIN)		RATIO H/D.	Mo ·	H/D.	L/D.
							*.	
	•						-	
2 00	B. 150	0.0120	0 2584	0 (500	0.0550	0.1413	0.0925	11.5836
		0.0120			0.0350	0.2350	0.1449	20.1100
		0.7120			0.1104	0.1139	0.1901	27.0405
		0.0120			0.1332	0.3533	0.2311	33.9907
10.00	0.150	0.0120	0.2586	0.0500	0.1544	0.4454	0.2698	40.0062
12.00	0.150	0.0120	0.2586	0.0500	0.1742	0.5039	0.3064	45.1237
								•
2 00	0.150	0.0120	0.6-66	0.0500	0.0440	0.2071	0.0925	13.2442
		0.0120			0.0448	0.3472	0.0425	22.4141
		0.0120			0.0894	0.4667	0.1901	30.7705
		0.9120			0.1075	0.2739	0.2311	37.3701
		0.0120			0.1244	0.6693	0.2698	44.6241
12.00	0.150	0.9120	0.5000	0.6500	0.1400	0.7605	0.3054	50.3003
3 00	0 150		0 3034	0 0500			0.0005	10 77.
				0.0500	0.0403	0.2546	0.0925	13.7751
		0.0120			0.0620	0.4290	0.1449	23.3326
		0.0120			0.0300 0.0963	0.5781	0.1901 0.2311	32.0156 39.3942
		0.0120			ŭ.1110	0.1099	0.2695	40.4021
		0.0120			0.1251	0.9445	J.3054	52.3635
				(00)	V Q Q C D D			115
		0.0120			0.037s	0.2873	0.0925	14.0445
		0.0120			0.0501	0.4853	0.1449	23.1773
		0.0120			0.0751	0.6533	0.1901	32.6333
		0.0120			0.0901 0.1041	0.5064	0.2311 0.2598	40.1849 47.3002
		0.0120			0.1170	1.0765	0.2090	54 4451
1200	04230		0.0000	0.0000	0.1170	1.0103	0.004	12
		0.0120			0.0365	0.3073	0.0925	14.1313
		0.0120			0.0562	0.5185	0.1449	2407203
		0.0120			0.0720	0.5991	0.1901	34.44,1
		0.0120			0.0871	0.6625	0.2311	40.5719 4/.53u3
		0.0120			0.1004	1.0138	0.2648 0.3064	47.83u3 53.9725
12.00	0.130	0.0120	0.7059	0.0000	0.1130	1.1528	0 • JUD 4	23.9125
	-							
2.00	0.150	0.C120	0.9962	0.0500		0.3123	0.0925	14.2135
		0.0120			0.0557	0.5277	0.1449	24.0534
		0.0120			0.0713	0.7131	0.1901	33.03.3
		0.9120			U. 0502	0.0792	0.2311	40.67.2
		0.0120			0.0914	1.0333	0.2045	47.9513
12.00	1.150	0.0120	0.9962	0.0500	6.1119	1.1751	0.3064	54.1153

2. 4. 6. 15.

FLOH L/S.	014.	MANN. COEFF	SUPPLY (SIN)	DFAIN SLUPE (SIN)	DRAIN FLOH ENTRY DEPTH RATIO H/D.	ENTRY ENERGY 1	NURMAL DEPTH H/O.	PIPE LENGTH TO NORMAL DEPTH: L/D:
4.00 6.00 8.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.2588 0.2588 0.2588 0.2588	0.0250 0.0250 0.0250 0.0250	0.0550 0.0351 0.1104 0.1332 0.1544 0.1742	0.1413 0.2350 0.3139 0.3533 0.4454 0.5039	0.1155 0.1825 0.2406 0.2942 0.3445 0.3933	15.7823 26.7455 30.1720 44.5354 51.4940 50.5004
4.00 6.00 8.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	9.5000 0.5000 0.5000 0.5000	C.C250 C.C250 C.U250 G.C250	0.0448 0.0692 0.0354 0.1075 0.1244	0.3472	0.1155 0.1325 0.2406 0.2942 0.3445 0.3933	10.9157 20.6935 30.d195 47.8755 55.3909 62.9923
4.00 6.00 8.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	9.7070 0.7070 9.7070 9.7070	0.0250 0.0250 0.0250 0.0250	0.0403 0.0620 0.0300 0.0963 0.1110 0.1251	0.2546 0.4290 0.5781 0.7099 0.0334 0.9448	0.1155 0.1325 0.2406 0.2942 0.3445 0.3933	17.4029 29.5321 39.9007 49.2594 57.0003 64.3930
4.00 6.00 9.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.5660 0.8660 0.8660 0.8660	0.0250 0.0250 0.0250 0.0250	0.0375 0.0551 0.0751 0.0901 0.1041 0.1170	0.2873 0.4053 0.6533 0.064 0.9453 1.0765	0.1155 0.1325 0.2406 0.2942 0.3445 0.3933	17.6544 27.9001 40.5420 50.0140 57.9500 60.9107
4.00 6.00 9.00 10.00	C.15C C.15C C.15C C.15C	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.9659 0.9659 0.9659 0.9659	0.0250 0.0250 0.0250 0.0250	0.0552 0.0726 0.0871	0.6991	0.1155 0.1825 0.2406 0.2942 0.3445 U.3933	17.7343 30.1555 40.8433 50.3030 50.4079 60.42.4
4.00 6.00 7.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.4962 0.4962 0.4962 0.4962	0.0250 0.0250 0.0250 0.0250	0.0557 0.0718 0.0462 0.0974	0.5277 0.7131 0.3792	0.1155 0.1525 0.2406 0.2942 0.3445 0.3953	17.7120 30.2403 40.9230 50.4703 50.5337

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FLOW	DIA.	HANN.	SUPPLY	DEAIN	DRAIN FLOW	ENTRY	NORMAL	PIPE LENGTH T
L/S.	. M.	CHEFF	SLOPE	SLOPE	ENTRY DEPTH	ENERGY	DEPTH	NORMAL DEPTH.
`	•		(SIN)	(SIN)	RATIO H/D	n.	H/D	L/D.
							3.1	
	-						144 144	
	135							
	14							
2.00	0.150	0.0120	0.2568	0.0125	0.0550	0.1413	0.1449	10.0761
4.00	0.150	0.0120	0.2568	0.0125	0.0551	0.2350	0.2311	30.4916
6.00	0.150	0-0120	0.2568	0.6125	0.1104	0.3139	0.3064	40.2251
8.00	0.150	0.0120	0-2586	0.0125	0.1332	0.3633	0.3707	48.6052
		0.0120			0.1544	0.4454	0.4436	55.6009
12.00	0.150	0.0120	0.2566	0.0125	0.1742	0.5039	0.5003	61.0543
				,				1
				0.0125	0.0448	0.2071	0.1449	19.1021
		0.0120	-		0.0692	0.3472	0.2311	32.3554
		0.)120			Ú.0894	0.4667	0.3064	42.7044
		0.3120			0.1075	0.5739	0.3767	51.8045
		0.0120			0.1244	0.0693		1010
12.00	0.150	0.0120	0-5000	0.0125	0.1400	0.7005	0.50×3	66.0021
					•			
					•			_
		0.0120			0.0403	0.2546	0.1449	19.6425
		0.0120			0.0620	0.4290	0.2311	33.18//
		0.0123			0.0806	0.5781	0.3064	43.9230
		0.3120			0.0953	0.7099	0.3767	53.2092
		0.0120			0.1110 .	0.6334	J.4430	60.3535
12.00	0.150	0.7120	0.7070	0.0125	0.1251	0.9448	0.5003	67.5715
2 00	0 150	0.0130	0 0440	0 0136	0 0273	0.3073	0.1440	10 6054
		0.0120 0.0120			0.0378	0.2873	0.1449	19.8956
		0.0120			0.0581 0.0751	0.4853	0.3064	46 67-6
		0.0120			0.0791	0.0064	0.3767	51 (1)213
		0.0120			0.1041	0.0004	0.4436	44 15.37
		0.0120			0.1170	1.0765	0.5063	47 7.17 W
12.00	00170	0.0120	0.0000	C. 0123	0.1110	1.0703	0.000	01.1211
					•			
2.00	0.150	0.0120	0.9659	0.0125	0.0365	0.3073	0.1449	20.0315
		0.0120			U. 0562	0.5188	0.2311	104-5613
		0.0120			0.0726	0.6991	0.3964	45.9432
		0.0120			0.0371	0.5625	0.3767	44.7053
		0.0120			0.1004	1.0138	3.4436	59-7534
		0.0120			0.1130	1.1528	0.5003	67.6375
								12,
2.00	0.150	0.0120	0.9962	C.0125	0.0362	0.3123	0.1449	20.1151
		0.0120			0.0557	0.5277	0.2311	120.9573
		0.0120			0.0718	0.7131	0.3064	40.21.4
		0.3120			5050.0	0.0792	0.3767	7703431
		0.0120			0.0994	1.0333	0.4436	54.63J3
12.00	0.150	0.0120	0.9962	0.0125	0.1119	1.1751	₩.5003	67.3570

6.0 6.0 6.0 10.0

100	./S.	CIA.	MANN. CUEFF	(21M) 2FG be 2nbbfa	CRAIN SLUPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LEIGTH II NORMAL DEPTH L/D.
	4.00 6.00 6.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.2566 0.2566 0.2566 0.2566	0.0167 0.0167 0.0167 0.0167	U.0550 U.0851 U.1104 U.1332 U.1544 U.1742	0.1413 0.2350 0.3139 0.3233 0.4454 0.5039	0.1320 0.2094 0.2766 0.3391 0.3937	17.7316 29.7515 39.3035 47.3573 50.5451 62.0543
1	4.00 6.00 8.00	0.150 0.150 0.150 0.150	0.9129 C.9120 0.9120 0.9129 C.9120 0.9120	0.5000 0.5000 0.5000 0.5000	0.0167 6.0167 0.0167 0.0167	0.0446 0.0692 0.0394 0.1075 0.1244 0.1400	0.2071 0.3472 0.4667 0.5739 0.6693 0.7605	0.1320 0.2094 0.2766 0.3391 0.3957 0.4558	10.8156 31.6205 41.9321 51.0969 59.3319 60.3907
1	4.00 6.00 8.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.7676 0.7676 0.7676 0.7670	0.0167 0.0167 0.0167	0.0403 0.0620 0.0300 0.0903 0.1110 0.1251	0.2546 0.4290 0.5781 0.7099 0.8334 0.9448	0.1320 0.2074 0.2766 0.3371 0.3987 0.4556	19.2535 32.4445 43.0659 52.4905 61.0163 60.2953
	4.00 6.00 8.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.8660 0.8660 0.8660	C.C167 C.C167 C.C167 C.C167	0.0375 0.0531 0.0751 0.0901 0.1041 0.1170	0.2873 0.4653 0.6533 0.6064 0.9453 1.0765	0.1320 0.2094 0.2706 0.3391 0.3967 0.4558	19.5303 32.8748 43.5000 54.2422 61.8003 69.3322
	4.00 6.00 6.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.0120 0.0120 0.0120 0.0120 0.0120	0.9659 0.9659 0.9659 0.9659	0.0167 0.0167 0.0167 0.0167	0.0365 0.0562 0.0726 0.0371 0.1304 0.1130	0.3073 0.5183 0.6991 0.5625 1.0133 1.1527	0.1320 0.2094 0.2766 0.3341 0.39.7 0.4528	19.5048 33.0931 43.9940 53.6150 62.3740 70.3171
ı	4.00 6.00 4.00 10.00	0.150 0.150 0.150 0.150	0.0120 0.1120 0.0120 0.1120 0.0120 0.0120	0.9962 0.9962 0.9962 0.9962	0.0157 0.0167 0.0167 0.0167	0.0352 0.0557 0.0710 0.0862 0.0974 0.1119		0.1320 0.2014 0.2766 0.3311 0.3967 0.4558	19.6723 33.1972 44.0414 53.7603 64.1293 71.5325

FLOW L/S.	DIA.	MANN. CJEFF	(SIN) STEAE SUBBEA	DEAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.			PIPE LENGTA NORMAL DEPT L/D.
							727 286	
	Fame.			:			· · ·	
2.00	0,150	0.0150	0.2588	C.6500	0.0633	0.1100	0.1068	8.6502
		0.0150			0.0982	0.1818	0.1681	14.6265
		0.0150			0.1278	0.2411	0.2211	19.7675
		0.0150			0.1544 0.1791	0.2934 0.3408	0.2698	24.4134 20.5509
		0.0150			0.2025	0.3408	0.3596	32.2764
12.00	00230	0.0170	0.2 300		0.2027	0.3037	0.33770	32.2704
2.00	C-150	0.0150	0.5000	0-0500	0.0515	0.1597	0.1068	9.0042
		0.0150			0.0797	0.2659	0.1601	16.2471
6.00	0.150	0.0150	0.5000	0.6500	0.1032	0.3557	0.2211	21.9764
		0.0150			0.1244	0.4351	0.2698	27.1350
		0.0150			0.1434	0.0076	0.3157	31.7375
12.00	0.150	0.0150	0.5000	0.0500	0.1022	0.5752	0.3596	35.9110
2 00	0 160	0.0150	0.7676	0.500	0.0462	0.1953	0.1068	9.9902
		0.0150			0.0714	0.1753	0.1000	16.9140
		0.0150			0.0923	0.4389	0.2211	22.9007
		0.0150			0.1110	0.5394	0.2648	20.2620
10.00	0.150	0.0150	0.7076	0.0590	0.1283	0.0309	0.3157	33.0702
12.00	C.150	C.0150	0.7070	0.0500	0.1447	0.7146.	0.3546	37.4100
2 00	0.356		0.044	6 65 66	0.0131	A 2201	0.30/0	10.10.2
		0.0150			0.0434 0.0670	0.2201	0.1068	10.1553 17.2543
		C. 0150			0.0070	0.4975	0.1551	23.3529
		0.0150			0.1041	0.6106	0.2698	28.5375
		0.0150			0.1202	0.7151	0.3157	33.7425
12.00	C.150	0.0150	0.8660	C.6500	0.1354	0.0114	0.3596	38.1436
2 00								20.2024
		0.0150			0.0420	0.2350	0.1068	10.2574 17.4305
		0.0150			0.0546 0.0336	0.3973	0.2211	23.5053
		0.0150			0.1004	0.0542	J. 2645	29.1343
		0.0150			6.1100	0.7552	0.3157	
		0.0150			0.1307	0.0670	0.3546	30.5703
	•							
			_	0.0500		0.2397	0.1008	10.3155
		0.0150 0.0150			0.0640	0.4026 0.5423	0.1631	17.47co 23.6525
		0.0150			0.0527 0.0594	0.5423	0.2698	29.2143
		0.0150			C.1148	0.7611	0.3157	34.1853
		0.01>0			0.1293	0.0869	J.3546	30.0713

Corr	FLOH	DIA.	MANN.	SHOEL V	DELTH	DRAIN FLOH	ENTRY	NURMAL	PIPE LENGTH
CSIP1 (SIN) RATIO H/D. H. H/D. L/D.									
2.00 6.150 0.0150 0.258e 0.0250	2734		90011			· ·		_	
2.00 %.150 0.0150 0.2588 0.0250									
4.00 0.150 0.0150 0.2558 C.2550 0.0902 0.1813 0.2123 10.0057 8.00 0.150 0.150 0.7586 C.2550 0.1273 0.2411 0.2910 24.1492 8.00 0.150 0.150 0.2586 C.2550 0.1544 0.2934 0.3445 29.2025 10.00 0.150 0.7150 0.2586 C.2550 0.1544 0.2934 0.3445 29.2025 12.00 0.150 0.7150 0.2586 0.0250 0.2025 0.3839 0.4631 37.5657 12.00 0.150 0.7150 0.5000 C.2560 0.0550 0.0757 0.3403 0.4631 37.5657 0.00 0.150 0.7150 0.5000 C.0250 0.0777 0.2659 0.2123 19.4694 8.00 0.150 0.7150 0.5500 C.0250 0.0777 0.2659 0.2123 19.4694 8.00 0.150 0.7150 0.5500 C.0250 0.0777 0.2659 0.2123 19.4694 8.00 0.150 0.7150 0.5500 C.0250 0.1032 0.3557 0.2310 26.0019 8.00 0.150 0.7150 0.5500 C.0250 0.1032 0.3557 0.2310 26.0019 8.00 0.150 0.7150 0.5500 C.0250 0.1244 0.4351 0.3445 31.5312 10.00 C.150 0.7150 0.5500 C.0250 0.1622 0.5752 0.4631 40.7793 12.00 C.150 0.7150 0.5000 C.0250 0.1622 0.5752 0.4631 40.7793 12.00 C.150 0.7150 0.5000 C.0250 0.1622 0.5752 0.4631 40.7793 12.00 C.150 0.7150 0.7070 0.0250 0.00462 0.1953 0.1337 11.9140 4.00 0.150 0.7070 0.0250 0.00462 0.1953 0.1337 11.9140 4.00 0.150 0.7050 0.7070 0.0250 0.00462 0.1953 0.1337 12.9140 8.00 0.150 0.0150 0.7070 0.0250 0.0014 0.3271 0.2123 26.9074 8.00 0.150 0.0150 0.7070 0.0250 0.0140 0.3271 0.2123 26.9074 12.00 0.150 0.0150 0.7070 0.0250 0.0140 0.3271 0.2123 26.9074 12.00 0.150 0.0150 0.7070 0.0250 0.0140 0.3271 0.2123 26.9074 12.00 0.150 0.0150 0.7070 0.0250 0.0140 0.3374 0.3445 32.4475 12.00 0.150 0.0150 0.7070 0.0250 0.0140 0.3374 0.3445 32.4475 12.00 0.150 0.0150 0.7070 0.0250 0.01447 0.7146 0.4351 42.2106 0.000 0.150 0.0150 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.3445 33.2014 0.000 0.150 0.0150 0.0000 0.0000 0.0000 0.0000 0.0000 0.3445 33.2014 0.000 0.150 0.0150 0.0000 0.0000 0.0000 0.0000 0.3445 33.2014 0.000 0.150 0.0150 0.0000 0.0000 0.0000 0.0000 0.0000 0.3445 33.2014 0.0000 0.150 0.0150 0.0000 0.0000 0.00000 0.0000 0.0000 0.3445 33.2014 0.0000 0.150 0.0150 0.0000 0.00000 0.0000 0.0000 0.3445 33.2014 0.0000 0.150 0.0150 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000									:
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8.00 0.150 0.0150 0.8660 0.6250 0.1041 0.6106 0.3445 33.2014 10.00 0.150 0.0150 0.8660 0.6250 0.1202 0.7151 0.4050 38.4704 12.00 0.150 0.0150 0.8660 0.6250 0.1354 0.3114 0.4631 42.9690									
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4.00 0.150 0.0150 0.9659 0.0250 0.0646 0.3953 0.2123 20.5863 6.00 0.150 0.0150 0.9659 0.0250 0.0836 0.5317 0.2510 27.5372 8.00 0.150 0.0150 0.9659 0.0250 0.1004 0.6542 0.3445 33.4321 10.00 0.150 0.2150 0.9659 0.0250 0.1160 0.7652 0.4050 36.2094 12.00 0.150 0.0150 0.9659 0.0250 0.1307 0.6678 0.4631 43.3456 2.00 0.150 0.0150 0.9962 0.0250 0.0415 0.2397 0.1337 12.2230 4.00 0.150 0.0150 0.9962 0.0250 0.0415 0.2397 0.1337 12.2230 6.00 0.150 0.0150 0.9962 0.0250 0.0640 0.4026 0.2123 20.6310 6.00 0.150 0.0150 0.9962 0.0250 0.0827 0.5423 0.2610 27.6028 5.00 0.150 0.0150 0.9962 0.0250 0.0827 0.5423 0.2610 27.6028 5.00 0.150 0.0150 0.9962 0.0250 0.0827 0.5423 0.2610 27.6028 5.00 0.150 0.0150 0.9962 0.0250 0.0344 0.0667 0.3440 33.5033									
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6.00 0.150 0.0150 0.9659 0.0250									
8.00 0.15C 0.0150 0.9659 C.C250 0.1004 0.6542 0.3445 33.4721 10.00 0.15C 0.0150 0.9659 C.C250 0.11c0 0.7652 0.4050 3c.t004 12.00 C.15C 0.0150 0.9659 C.C250 0.1307 0.6678 0.4631 43.3456 2.00 0.15C 0.0150 0.9962 C.C250 0.0415 0.2397 0.1337 12.2270 4.00 C.15C 0.0150 0.9962 C.C250 0.0640 0.4026 0.2123 20.6316 6.00 C.15C 0.0150 0.9962 C.C250 0.0827 0.5423 0.2610 27.6028 5.00 C.15C 0.0150 0.9962 C.C250 0.0827 0.5423 0.2610 27.6028 5.00 C.15C 0.0150 0.9962 C.C250 0.0827 0.5423 0.2610 33.7673 10.00 0.15C C.0150 0.9962 C.C250 0.1148 0.7811 0.4050 30.7039									
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2.00 0.150 0.0150 0.9962 0.6250 0.0415 0.2397 0.1337 12.2270 4.00 0.150 0.9962 0.6250 0.045 0.4626 0.2123 20.6310 6.00 0.150 0.9962 0.6250 0.0827 0.5423 0.2610 27.0728 5.03 0.150 0.9962 0.6250 0.0827 0.5423 0.2610 27.0728 5.03 0.150 0.9962 0.6250 0.0974 0.0667 0.3445 33.7673 10.00 0.150 0.9962 0.6250 0.1148 0.7811 0.4050 30.733									
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4.00 0.150 0.0150 0.9962 0.0250 0.0640 0.4026 0.2123 20.6315 6.00 0.150 0.0150 0.9962 0.0250 0.0827 0.5423 0.2610 27.6526 5.03 0.150 0.0150 0.9962 0.0250 0.0394 0.0667 0.3445 33.5693 10.00 0.150 0.0150 0.9962 0.0250 0.1148 0.7811 0.4050 30.9339									
4.00 0.150 0.0150 0.9962 0.0250 0.0640 0.4026 0.2123 20.6315 6.00 0.150 0.0150 0.9962 0.0250 0.0827 0.5423 0.2610 27.6526 5.03 0.150 0.0150 0.9962 0.0250 0.0394 0.0667 0.3445 33.5693 10.00 0.150 0.0150 0.9962 0.0250 0.1148 0.7811 0.4050 30.9339	2.00	0.150	0.0150	0.9962	0.6250	0.0415	0.2397	0-1337	14.2210
6.00 C.15C 0.0150 0.9962 C.C250									
5.00 (.150 0.0150 0.4962 (.0250 0.0474 0.0667 0.3445 33.5693 10.00 0.150 (.0150 0.4962 0.0250 0.1148 0.7811 0.4050 30.7039									
10.00 0.150 (.0150 0.4962 0.6250 0.1148 0.7811 0.4050 30.7334									
12.00 0.150 0.7150 0.4462 0.0250 0.1293 0.0869 0.4631 43.4034						0.1140			30.7337
	12.00	0.150	0.1150	0.4462	0.0250	0.1293	0.0869	0.4631	43.4034

FLOW L/S.	ola.	MANN. COEFF	SUPPLY SLOPE (SIN)	DRAIN SLGPE. (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY EHERGY	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPI L/D.
2.00	0.150	0.0150	0.2586	0.0167	0.0633	0.1100	0.1527	11-0444
		0.0150			0.0902	0.1818	0.2438	10.3513
		G.0150	-		0.1276	0.2411	0.3240	24.0826
		0.0150			0.1544	0.2934	0.3967	26.7185
		0.0150 G.0150			0.1791	0.3408	0.4700	32.5011 35.48JZ
12.00	0.150	6.7150	0.2568	0.0167	0.2025	0.3039	0.7300	37.4072
2.00	0.150	0.0150	0.5000	0.0167	0.0515	0.1597	0.1527	11.3447
		0.0150			0.0747	0.2659	0.2438	19.7273
		C.0150			0.1032	0.3557	0.3240	25.9744
		0.0150			0.1244	0.4351	0.3957	31.0713
		C. 0150			0.1439	0.5075	0.4700	35.2815
12.00	0.150	0.7150	0.5000	0.0157	0.1622	0.5752	0.5306	30.5815
2.00	0.150	0.0150	0.7076	C.0167	0.0462	0.1953	0.1527	12.2030
		0.3150			0.0714	0.3271	0.2438	20.3510
		0.0150			0.0923	0.4389	0.3240	20.8200
. 8.00	0.150	0.0150	0.7070	0.0167	0.1110	0.5394	0.3957	32.1454
		0.0150			0.1283	0.6309	0.4700	36.5600
12.00	0.150	0.0150	0.7676	0.6167	0.1447	0.7146	0.5386	40.1353
2.00	0.150	0.0150	0.8640	0.6167	0.0434	0.2201	0.1527	12.3439
		0.0150			0.0670	0.3694	0.2438	20.6810
		0.3150			0.0865	0.4975	0.3240	27.2899
		0.0150			0.1041	0.6106	0.3957	32.7123
		0.0150			0.1202	0.7151	0.4700	37.2303
12.00	0.150	0.0170	0.8660	C.0167	0.1354	0.8114	0.5366	4ú. 9677
2 00	0 150	0.0150	0.0450	. 0147	0.0630	0.2350	0.1527	12.4929
		0.0150			0.0420	0.2350	0.1327	20.8547
		0.0150			0.0040	0.5317	0.3240	27.52.4
		0.0150			0.1004	0.6542	0.3957	33.2450
		G. 0150			0.1160	0.7652	0.4700	31.3540
12.00	0.156	0.0150	0.9659	C.C167	0.1307	0.3678	0.5356	41.5034
							•	
2.00	0.150	0.0150	0.9962	0.0167	0.0415	0.2397	0.1527	12.5218
		0.0150			0.0040	0.4026	0.2438	20.9003.
		0.0150			0.0327	0.5423	0.3240	27.5877
		0.7150			0.0944	0.0667	0.3957	33.3315
		0.0150			0.1143	0.7611	0.4700	28.9021
12.00	0.150	0.0150	0.9962	0.0167	0.1293	0.3669	0.5336	41.5045

			-			•		
FLOH L/S.	DIA.	MANN. COEFF	STCLE STCLE	DRAIN SLUPS (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPT L/O.
							2 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	
			0.2586		0.0633 0.0982	0.1100 0.1516	0.1661 0.2699	10.3052 16.9455
			2.2560		0.1276	0.2411	U.3596	21.6594
3.00	0.150	0.0150	0.2528	0.0125	0.1544	0.4934	0.4436	24.4771
			0.2586		0.1791	0.3405	. 0.5239	27.5034
12.00	C.15C	0.9150	0.2566	0.0125	0.2025	0.3839	0.6021	30.1773
			0.5000		0.0515	0.1597	0.1681	11.1153
			0.5000		0.0797	0.2659	0.2698	16.3369
			0.5000		0.1032 0.1244	0.3557	0.3596 0.4436	23.6036 27.3473
			0.5000		0.1439	0.5076	0.5239	30.3022
			0.5000		0.1622	0.5752	0.6021	34.6502
2.00	0.150	0.0150	0.7070	0.0125	0.0462	0.1953	0.1681	11.4820
			C.7C7C		0.0714	0.3271	0.2698	10.9751
			0.7676		0.0923	0.4389	0.3596	24.4751
			0.7070		0.1116 G.1283	0.5394	0.4436 0.5239	28.4426 31.6555
			0.7070		0.1447	0.7146	0.6021	33.4417
2.00	0.150	0.0150	0.8660	C.C125	0.0434	0.2201	0.16:1	11.67.2
4.00	0.150	0.0150	0.2660	0.0125	0.0670	0.3694	0.2698	19.2587
			0.8660		0.0265	0.4975	0.3596	24.8705
			0.86.0		0.1041 0.1202	0.6106	J.4436 U.5239	29.0154 32.3535
			0.8660		0.1354	0.7131	0.6021	34.0346
2.00	0.150	C.0150	0.9659	0.0125	0.0420	0.2350	0.1681	11.83/1
			0.9659		0.0640	0.3953	0.2698	19.3509
			0.9659		0.0335	0.5317	0.3546	25.36.6
			0.9659		0.1904 0.1160	0.0542	U.4436 U.5239	29.3223 32.7923
			0.5659		0.1307	0.1032	0.5234	34.9721
2.00	0.150	0.3159	0.9962	C.C125	U.0415	0.2397	0.1661	11.9053
4.00	0.150	0.0150	C.9942	0.0175	0.0640	0.4026	0.2698	19.3750
			0.9462		0.0327	0.5423	0.3596	25.1246
			0.9962		0.0094	0.0667	0.4436	24.4033
			0.9962		0.1145 0.1273	0.7±11 0.4864	0.6021	3220 35.1037
22.00	0.100	0.7270	0. 1702	0.0127	0 0 1 2 7 3	0.0007	0.0021	33.1037

	GIA. M.	MANY. COEFF	SUPPLY SLOPE (SIN)	DFAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RAILO H/D.	ENTRY EHERGY M.	NORMAL DEPTH H/D+	PIPE LENGTH NURMAL DEPT: L/O.
						-	•	:
	- -						•	•
Э		0.0140	0.2586	0.0500	0.0710	0.0906	0.1201	6.4405
Ú	0.150	0.3130	0.2568	0.0500	0.1104	0.1487	0.1901	11.0069
			0.2588		0.1439	0.1966	0.2507	14.7576
			0.2588		0.1742	0.2335	0.3064	17.3602
			0.2560		20.2025	0.2759	0.3546	20.9155
O	0-150	0.3140	J.2586	0.0500	. U . 2294	0.3100	0.4104	23.4247
0	0 150	0.0180	0.5000	0 0500	0.0577	0.1296	0.1201	7.1413
			0.5000		0.0074	0.2149	0.1901	12.1955
			0.5000		0.1100	0.2666	0.2507	16.3812
			0.5000		0.1400	0.3497	0.3004	14.5475
			0.5000		U. 1022	0.4069	0.3540	23.2511
0	0.150	0.0130	9.5000	0.0500	0.1035	0.4582	0.4104	20.9627
			0.7070		0.0518	0.1579	0.1201	7. 4375
			0.7070		0.0500	0.2636	0.1901	12.7054
			0.7070		0.1036 0. 1251	0.3518	0.2507 0.3064	17.0650 20.7004
			0.7070		0.1447	0.5028	0.3596	- 24 • 257 o
			0.7(76		0.1032	0.5685	0.4104	27.2255
			0.8660		0.0466	0.1777	0.1201	7.5925
			0. Et & U			0.2966	0.1931	12.9649
			0.8666		0.0472	0.1980	0.2507	17-4218
			0.8660		0.1170	0.4582	0.3064	21.1591
			0.6660		0.1354	0.5697	0.3576	24.7550
U	0.150	0.7150	0.8660	0.0500	0.1527	0.6445	0.4104	27.3291
) Û	0.150	0.0130	0.9659	0.0500	0.0470	0.1896	-0-1201	7.6719
			0.9659		0.0726	0.3169	0.1931	13.0445
10	0.150	0.0140	0.9659	0.0500	0.0738	0.4259	0.2507	17.6157
13	C.15C	0.0130	0.4654	0.6500	U-1130	0.5213	U.3054	21.3053
			0.4659		0.1307	0.6035	0.3596	25.0474
) 0	0.150	0.71,0	0.9657	C. 6500	0.1473	0.5899	0.4104	28.1325
30	0.160	0.0140	0.9962	0.6500	0.0465	0.1929	0.1201	7.5924
			0.9962		0.0710	0.1929	0.1901	13.1379
			0.9962		0.0718	0.4334	0.2507	17.5032
			0.4962		0.1119	0.5315	0.3004	21.4457
			0.9962		0.1293	0.6218	0.3596	25.13.2
10	0.150	0.31:0	0.4962	C. (500	0.1459	0.7032	0.4104	20.21-1

100	FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLCPE (SIN)	DPAIN SLLPF (SIH)	DRAIN FLUH ENTRY DEPTH RATIO H/D.	ENERGY	NURMAL DEPTH H/D.	PIPE LENGTH TO NORMAL JEPTH. L/O.
	4.00 6.00 8.00	0.150 0.150 0.150 0.150	0.0130 0.0130 0.0130 0.0130	0.2560 0.2588 0.2588 0.2580 0.2580 0.2588	C.6250 C.6250 C.6250 O.6250	0.0710 0.1104 0.1439 0.1742 0.2025 0.2294	0.0906 0.1487 0.1966 0.2385 0.2759 0.3100	0.1508 0.2406 0.3190 0.3933 0.4631 0.5308	7.3353 12.2103 16.0155 19.1605 21.57/3 23.5905
1986	4.00 6.00 8.00 10.00	0.150 0.150 0.150 0.150	0.0130 0.0130 0.0130 0.0130	0.5000 0.5000 0.5000 0.5000 0.5000	0.0250 C.0250 G.0250 C.0250	0.0577 0.0394 0.1160 0.1400 0.1522 0.1535	0.1296 0.2149 0.2066 0.3447 0.4369 0.4582	0.1508 0.2406 0.3146 0.3933 0.4531 0.5306	7.9435 13.2053 17.4614 20.9520 23.6594 26.6046
	4.00 6.50 8.00 10.00	0.150 0.150 0.150 0.150	0.0130 0.0130 0.0130 0.0130	0.7070 0.7070 0.7070 0.7070 0.7070	0.0250 0.0250 0.0250 0.0250	0.0518 0.0800 0.1038 0.1251 0.1447 0.1632	0.1579 0.2636 0.3518 0.4303 0.5625 0.5668	0.1508 0.2406 0.3176 0.3933 0.4631 0.5300	6.2235 13.7521 16.1153 21.7645 24.0770 27.1353
	4.00 0.00 3.00 10.00	C.15C C.15C C.15C C.15C	0.0130 0.0130 0.0130 0.0130	0.8660 0.7660 0.2660 0.8660 0.8660	0.0250 0.0250 0.0250 0.0250	0.04db 0.0751 0.0972 0.1170 0.1354 0.1527	0.41777 0.2965 0.3980 0.4652 0.5697 0.6446	0.1503 0.2406 0.3190 0.3933 0.4631	8.3739 14.0002 16.4771 22.2209 25.2014 27.7374
200.00	4.00 5.00 3.00 10.00	0.150 0.150 0.150 0.150	0.0150 0.0150 0.0150 0.0130	0.4659 0.9659 0.9659 0.9659	C.C250 C.C250 C.C250 O.C250	0.0726	0.1896 0.3168 0.4259 0.5216 0.0065 0.5899	0.1508 0.2406 0.3176 0.3933 0.4631 0.5308	8.4553 14.1375 10.6533 24.4577 25.4552 20.0462
	4.00 6.00 1.00	0.150 0.150 0.150 0.150	0.2130 0.2130 0.2130 0.2130 0.3130	0.9962 0.9962 0.9962 0.9662 0.9662	0.0259 0.0250 0.0259 0.0259	0.0713 0.0930 0.1119 0.1273	0.1929 0.5229 0.4334 0.5316 0.5215 0.7032	J.3933 U.4631	6.4770 14.1775 16.7075 24.5073 25.553 25.553

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY	SLCPE	DRAIN FLOW ENTRY DEPTH	ENTRY ENERGY	NOKMAL DEPTH	PIPE LEAGTH T
			(SIN)	(RIZ)	RATIO H/D.	n.	H/D.	L/9.
	•							:
	84							
2.00	0-150	0.0130	0.2588	0.0167	0.0710	0.0906	0.1725	6.5632
4.00	0.150	0.0180	0.2588	0.6167	0.1104	0.1487	0.2766	10.6332
6.00	0.150	0.0130	0.2566	0.0167	0.1439	0.1966	0.3644	13.3740
		0.0130			0.1742	0.2385	0.4558	15.3170
		0.0130			20-2025	0.2759	0.5306	15.9317
12.00	0.150	0.0130	0.2588	0.0167	0.2294	0.3100	0.6146.	16.8905
				,				
2.00	0.150	0.0130	0.5000	0.0157	0.0577	0.1296	0.1725	7.1765
		0.3130			0.0894	0.2149	0.2766	11.6726
		0.0130			U.1160	0.2865	0.3694	14.0100
		0.7110			0.1400	0.3497	0.4550	16.9556
		0.0130			0.1022	0.4069	0.5300	17.4543
12.00	0.150	0.013.0	0.5000	0.6167	0.1d35	0.4582	0.6196	14.4444
2.00	0.150	0.0130	0.7676	0.6157	0.0518	0.1579	0.1725	7.4623
		0.7130			0.0800	0.2636	0.2766	12.1/15
		0.0130				0.3518	0.3694	15.4874
		0.7130			0.1251	0.4303	0.4558	17.7015
10.00	0.150	0.0130	0.7070	0.0167	0.1447	0.5028	0.5386	17.7407
12.00	0.150	0.3130	0.7070	C.0157	0.1632	0.5688	0.6196	20.4805
				•				
2.00	0-150	0.0130	0.8660	0.6167	0.0486	0.1777	0.1725	7.6178
		0.9130				0.2966	0.2750	12.4540
6.00	0.150	0.0130	0.8660	C.0167	0.0972	0.3980	0.3694	15.3547
8.00	0.150	0.0130	0.8660	C. 0167	0.1170	0.4882	0.4558	10.1373
		0.0130			0.1354	0.5697	0.5336	17.48/7
12.00	0.150	0.7100	0.5660	0.0167	U.1527	0.0445	0.6146	21.9213
								1
2.00	0.150	0.0130	0.9659	C.C167	0.0470	0.1996	0.1725	7.6935
		0.0150			U.0726	0.3165	0.2766	12.5924
6.00	0.150	0.0130	0.9659	C. C167	0.0936	0.4259	0.3694	16.0401
8.00	0.150	0.0150	0.9654	C. 0167	0.1130	0.5218	0.4555	15.3957
		0.0130			0.1307	0.0086	0.5306	17.0537
12.00	0.150	0.0130	0-9659	0.6167	0.1473	0.0599	0.6146	21.2955
2.00	0.150	0.0130	0.9962	C.0167	0.0465	0.1929	0.1725	7.7194
		0.0130			0.0710	0.3229	0.2766	12.6321
		0.0130			0.0930	0.4334	0.3694	10.0941
		0.0130			0.1119	0.5315	0.4558	10.4503
		0.1137			0.1293	0.0216	0.5336	16.3390
12.00	C.150	0.0130	0.9962	C.0167	0.1479	0.7032	0.6176	21.3742

FL'		DIA.	MANN. CDEFF	SUPPLY SLOPE (SIN)	DRAIN SLUPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPT L/D.
								70 e	:
2	-00	0.250	0-0070	0.2568	C.6500	0.0460	0.1973	0.0770	17.4232
				0.2586		0.1593	0.3015	0.2791	76.2177
				0.2568		0.1742	0.8755	0.3064	83.2054
				0.2566		0.1856	0.9454	0.3333	90.6257
				0.2568		0.2025	1.0123	0.3596	96.14.7
22	.00	0.150	0.7970	0.2588	0.0500	v.2102	1.0750	0.3850,	103.71+0
				0.5000		0.0375	0.2919	0.0770	19.4863
	-			0.5000		0.1233	1.2181	0.2791	85.0579
				0.5000		0.1400	1.3357	0.3064	92.9312
				0.5000		0.1515	1.4441	0.3333	101.1729
_				0.5000		0.1622 0.1730	1.5545	0.3596 0.3850	109.5392 115.8832
~ ~	• • • •	0.170	0.0070	0.000	(20) 0 9	0.1730	140340	0.3030	117.0032
				0.7070		0.0337	0.3592	0.0770	20.2637
				0.7070		0.1147	1.5175	0.2791	86.4630
				0.7070		0.1251	1.6651	0.3004	96.6575
				0.7676		0.1351 0.1447	1.9463	0.3333	105.3029 113.9653
				0.7070		0.1542	2.0731	0.3850	120.6412
		00270	00,000	001010	(• 0) 0 0	0.1712	2.0131	003370	22000122
				0.8660		0.0316	0.4069	0.0770	20.6619
				0.8660		0.1074	1.7281	0.2741	90.2155
				0.8660		0.1170 0.1263	1.9002	0.3064	90.6440 107.4270
				0.8000		0.1263	2:2177	0.3596	116.2043
				0.8660		0.1442	2.3662	0.3850	123.0747
2	.00	0.150	0.0000	0.9659	C. 0500	0.0306	0.4344	0.0770	20.0545
				0.9659		0.1037	1.0506	0.2741	91.0693
				0.9659		0.1130	2.0363	0.3004	94.5937
				0.9659		0.1220	2.2096	V • 3333	100.4529
				0.9659		0.1307 0.1390	2.3757	0.3596 0.3850	117.3021 124.2983
٤ ۷	• • •	0.130	0.0070	0.7079	0.0500	0.1390	2.5415	0.3070	124.273
2	.00	0.150	0.0030	0.9962	0.6500	0.0303	0.4426	0.0770	20.9075
14	.00	C.150	0.0010	0.9962	0.0500	0.1026	1.8599	0.2791	91.3227
	-			0.9962		0.1119	2.0759	0.3064	95.0003
				0.4464		U.120c	2.2539	0.3333	105.7313
				0.4962		0.1293	2.4292	0.3546	117.0457
65	.00	0.150	0.3033	0.9962	0.0520	U.1376	2.5953	0.3850	124.6451

FLOW L/S.	CIA.	MANN. COEFF	SUPPLY SLCPE (SIN)	DEAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH PATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH TO NORMAL DEPTHO L/Jo
								:
								· ·
2 00						0 1070	0.0010	24 4 277
·		0.0030			0.0460 0.1593	0.1973	0.0960 0.3567	24.4377 102.7d>5
		0.0010			0.1742	0.3015	0.3933	113.07:3
		0.0070			J.1550	0.9454	0.4205	124.0241
		0.0000			0.2025	1.0123	0.4631	130.47,2
		0.3073			₹.21o2	1.0750	J. 4976 .	
				•				
		0-0030			0.0375	0.2919	0.0900	26.1320
		0.1070			0.1203	1.2181	0.3507	110.2357
		0.7070			0.1400	1.3357	0.3933	121.8557
		0.0010			0.1515	1.4441	0.4255	130.4347
		0.0090			0.1622 0.1730	1.5545	0.4631 0.4976	140.15J4 149.7175
22.00	(.150	0. 104.5	0.2680	0.0250	0.1730	1.6545	0.4916	144.1115
2.00	0.150	0.0000	3.7676	C. 0250	0.0337	0.3592	0.0960	26.5259
		0.3370			0.1147	1.5175	0.3567	113.3500
		0.0070			0.1251	1.0651	0.3933	125.26/2
18.00	0.150	0.0090	0.7076	0.0250	0.1351	1.3066	U.4235	134.7235
		0. 2030			0.1447	1.9463	0.4531	144.2312
22.00	0.150	0.0090	0.7676	0.0250	U.1542	2.0731	0.4976	154.0736
2 00	0 150	0.0000	2 8440	C (250	ú.0316	0.4069	0.0960	27.1915
		0.7073			0.1074	1.7281	0.3567	115.0039
		0.0000			0.1176	1.4002	0.3933	127.94.2
		0.0090			0.1263	2.0025	9.4235	136.7224
		0.0000			0.1354	2.2177	0.4631	140.3530
		0.0090			6.1442	2.3662	0.4976	150.3614
		0.0073			0.0306	0.4344	0.0960	27.3757
		0.0090			0.1037	1.0506	0.3507	115.3170
		0.0000			0.1130	2.0363	0.3933	127.9900
		(.) (.)			0.1220 0.1307	2.2090	0.4235	137.69.4
		0.0070			0.1390	2.3/3/	0.4631 0.4976	147.4040 157.5251
22000	0.170	0 6 75 75	00 7657	(10 2) (0 - 1370	2.07417	0.4770	17107651
2.00	0.150	0.0090	0.9962	C.0250	0.0303	0.4426	0.0900	27.42.2
		0.1070			0.1026	1.0094	0.3567	116.0500
		0.0010			0.1119	2.0759	0.3433	125.2342
		0.0010			0.1208	2.2539	0.4245	137.9727
		0.3010			0.1243	2.4292	0.4011	147.7353
22.00	0.150	0.3330	0.4462	0.0250	u.1376	2.5453	J.4976	157.0070

FLOH L/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIM)	DEAIN SLIPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY	NURMAL DEPTH H/D.	PIPE LEAGTH TO NORMAL DEPTH. L/U.
	•						••	
	<u>.</u>							
2.00	0-15 C	0.0090	0.2588	0.0167	0.0460	0.1973	0.1093	26.3700
		0.7010			0.1593	0.5015	0.4133	117.6033
		0.0000			0.1742	0.0755	0.4558	127.4747
		0.3330			0.1856	0.4454	0.4976	136.7757
		0.3030			0.2025	1.0123	0.5306	145.3435
22.00	0.150	0.0090	0.2566	0.0121	0.2162	1.0750	0.5716	155.5575
				,				2
		0.2020			0.0375	0.2919	0.1093	29.9749
-		0.0070			0.1203 0.1400	1.2181	0.4133	124.7853
		0.0090			0.1515	1.4441	0.4976	145.5512
		0.1010			0.1622	1.5545	0.53=6	150.20.0
		0.0090			0.1730	1.6546	0.5796	165.53.5
		٠			•			12
2.00	0.150	0.0030	0.7070	C. 0167	0.0337	0.3592	0.1093	30.6478
		0.0010			0.1147	1.5175	0.4133	127.2375
		0.0000			0.1251	1.6651	0.4558	130.7596
		0.0070			0.1351	1.3066	0.4976	144.3213
		0.3330			0.1447	1.4463	0.5336	159.2400
22.00	0.15C	0.7999	0.7076	C.0167	0.1542	2.0731	0.5776	164.9419
								50
2.00	0.150	0.0090	0.8660	0.0167	0.0316	0.4069	0.1093	31. 3059
		0.0090			0.1074	1.7281	0.4133	129.4513
		0.0090			C-1170	1.9002	0.4558	140.5025
		0.0010			0.1263	2.0625	0.4976	151.3129
		0.3370			0.1354	2.2177	0.5336	161.3573
22.00	0.150	0.0090	0.8660	€.6167	G.1442	2.3662	0.5776	170.8626
								31.1456
				C.C167	0.0366	0.4344	0.1093	32.02.70
		0.0090			0.1037	1.0506	0.4133	130.2003
		0.0090			0.1130 0.1220	2.0363 2.2096	0.4976	143.4414
		0.0070			0.1220	2.3757	0.53.6	104.7523
		0.3173			0.1340	2.5415	0.5746	167-5537
								1e, 20,
2.00	0.150	0.0190	0.9962	0.0167	.0.0303	0.4426	0.1093	31.2345
		0.7010			0.1026	1.8894	0.4133	124.4370
		0.2010	-		0.1119	2.0757	0.4550	145.1751
		0.1070			U. 1203	2.2539	0.4976	150.3111
		0. 2222			0.12/3	2.4292	0.53=0	160.1333
22.00	0.150	0.0070	0.4962	0.6167	0.13/0	2.5953	0.5770	100.00 11

14, 16, 13, 20,

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	FLUM	DIA.	MANN.	SUPPLY		DRAIN FLOH		NORHAL	PIPE LENGTH TO
i	L/S.	F .	COEFF	SLGPE	SLCPF	ENTRY DEPTH		DEPTH	NORMAL DEPTH.
		•		(\$16)	(SIN)	RATIO H/D.	' H.	H/D.	L/U.
many many									
	2.00	0.150	0.0090	3355.0	0.6125	0.0460	0.1973	0.1201	30.8745
-	14.00	0.150	0.0070	0.2560	0.0125	0.1543	0.3615	0.4597	124.7729
				3.2586		0.1742	0.0755	0.5033	130.1535
r	19.00	0.150	0.2010	0.2588	C.C125	0.1936	0.7454	0.5552	145.00/9
l				0.2586		0.2025	1.0123	0.6021	154.5910
				0.2560		U.2162	1.0750	0.6479	162.9501
l									
					•				
	2.00	0.150	0-2030	0.5000	0-6125	u.0375	0.2919	0.1201	32.4492
				0.5000		0.1253	1.2181	0.4597	131.3374
				0.5000		0.1400	1.3357	0.5033	143.7535
				0.5000		0.1515	1.4441	0.5552	153.5332
				0.5000		0.1622	1.5545	0.6021	163.4321
				0.5(00		0.1730	1.0546	0.5479	172.5004
	22.00	00170	0.5775	0.5(00	(• • • • • •	,081130	100740	0 0 0 1 1 7	1720000
							•		
	2 00	0 150	0 2020	0.7070	6 6125	0.0337	0.3592	0.1201	33. 12v3
				0.7070		6.1147	1.5175	0.4597	137.3500
				0.7070		Ú-1251	1.6651	0.5003	146.3209
				0.7070		0.1351	1.5055	0.5552	
									163.9750
				0.7076		0.1447	1.9463	0-6021	164.1053
	22.00	0.150	0. 1.19)	0.7070	0.0125	0.1542	2.0731	0.6479	171.6434
	2 00	0 150	0.0000	0.8666	0 (125	0 0214	0.4069	0.1201	22 47 .2
				0.2666		0.0316			33.47.43
				0.8666		0.1074 0.1170	1.7281	0.4597	150.3715 145.1407
							1.9002	0.5003	
				0.8660		0.1263	2.0625	0.5552	175.9994
				0.1660		0.1354	2.2177	0.6021	166.7457
	22.00	0.150	0. 1010	0.8660	0.6125	0.1442	2.3862	0.6419	167.6553
	2 00	0 150	0.0000	0.9654	((.135	6 0304	0.6364	0.1201	22 4b- 2
				0.9659		0.0306	0.4344	0.1201	33.6552
				0.9659		0.1037	1.0505	0.4547	160.9155
				0.9659		0.1130	2.0363	0.5003	144.5337
						0.1220	2.2095	0.5552	180.4150
				1).9+59		0.1307	2.3757	3.5021	159.357
	22.00	0-150	0.7775	0.4654	0.0175	0.1340	2.5415	J. 6474	165.5757
	2 02	0.360	() 2012	0.054	0 (2.34		0 ((3)	0 1301	20.20.2
				0.9962		0.0303	0.4426	0.1201	33.7053
				0.9462		0.1026	1.5599	0.4547	172.00.4
				0.4962		0.1119	2.0759	Ü-5083	144.3517
				0.4462		0.1208	2.2539	0.5552	180.5113
				0.9962		0.1293	2.4292	0.0021	150.54.2
	22.00	0.150	0.1073	0.5462	C.C.125	L.1376	2.5953	0.6479	160.0034

FLOW L/S.	CIA.	HANN. COEFF	SUPPLY SLCPE (SIN)	DRAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/O.	PIPE LENGTH TO MORMAL DEPTH. L/D.
							# - # b	
							• • •	
2.00	0-150	0.0120	0.2588	0-0500	0.0550	0.1413	0-0925	11.8886
			0.2588		0.1932	0.5574	0.3420	50.3711
			0.2568		0.2115	0.6077	0.3767	52.35/0
			0.2568		0.2294	0.6544	0.4194	59.777)
			0.2566		0.2458	0.6930	.0.4436	64.2444
22.00	0.150	0.0120	0.2566	0.6500	0.2634	0.7417	0.4758	67.3275
							•	
	_		ė					
			0.5000		0.0440	0.2071	0.0925	13.2442
			0.5000		0.1552	0.0430	0.3420	50.1251
			0.5000		0.1696	0.4219	0.3767	61.6334
			0.5000		0.1835	0.9966	0.4104	66.63J5 71.6370
			0.5000		0.1969 0.2101	1.0683	0.4436 0.4756	75.0052
22.00	0.150	0.0120	0.5000	0.0500	0.2101	1.1330	0.775	17.8652
								2
2.00	C-15C	0.0120	0.7070	0.0500	0.0403	0.2546	0.0925	13.7751
			0.7076		0.13:3	1.0523	0.3440	50.4000
			0.7670		0.1510	1.1530	0.3707	64.2400
			0.7070		0.1632	1.2491	0.4104	64.4318
20.00	0.150	0.0120	0.7076	C.C500	0.1752	1.3387	0.4436	74.0295
22.00	0.150	0.7120	0.7070	0.0500	Ú.1369	1.4232	0.4758	78.5002
								1 2
_							_	
			0.8666		0.0378	0.2873	0.0925	14.0445
			0.6660		0.1275	1.1958	0.3420	59.6354
			0333.0		0.1412	1.3133	0.3767	65.5550
			0.8666		0.1527	1.4217	0.4104	70. 3424
			0.8666		0.1637 0.1744	1.5274	0.4436 0.4758	70.16.2 80.5357
22000	0.150	0.0 177 0	0.0000	0.0550	0.1744	1.0275	0.4770	20
								22
2.00	0.150	0.0120	0.9659	0.0500	0.0365	0.3073	0.0925	14.1313
			0.9659		0.1249	1.2841	0.3420	66-2471
16.00	0.150	0.1120	0.9659	(. 05 70	0.1304	1.4067	0.3767	65.19/5
			0.9659		0.1473	1.5247	0.4104	71.7743
			0.9659		0.1570	1.0402	J.4436	70.9440
22.00	0.150	0.7120	0.9659	0.6500	0.1633	1.7449	0.4758	81.3473 10 20
2 00		0 0000	0.00:1	0.0500		0 2122	0.0035	
			0.9962		0.0362	0.3123	0.0925	14.2135
			0.99(2		0.1237	1.3090	0.3420 0.3707	60.4003
			0.9962		0.1349 U.1459	1.4368	0.4104	71.74/5
			0.9962		0.1564	1.6704	0.4436	77.1373
			0.4462		0.1606	1.7501	0.4755	01.0740
22.00	00170	00.77.0	76 7702	0.00 7.70	0.1000	10.001	004170	22

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FLOW L/S.	DIA.	MANN. C'JEFF	SUPPLY SLEPE (SIN)	SLUPE	DRAIN FLOW ENTRY DEPTH RATIO M/D.	ENTRY ENEPGY	NURMAL DEPTH H/O.	PIPE LENGTH TO NORMAL DEPTH: L/O.
2 00	0.150	0.0120	0 2566	C . C2 50	0 • 05 50	0.1413	0.1155	15.7823
		0.0120			0.1932	0.5574	0.4402	
		0.3120			0.2115	0.6077	0.4501	69.3542
		0.7120			0.2294	0.0544	0.5308	74.5447
	-	0.7120			0.2408	0.6980	0.5353	60.11/3
		0.7120			0.2634	0.7417	0.6107	83.6444
22.00	(*150	0.7120	0.2360	(.02)0	0.2034	0.1411	0.0107	03.0744
			É	*				
2.00	0.150	0.0120	0.5000	0.0250	0.0448	0.2071	0.1155	16.9157
		0.0120			0.1552	0.6430	0.4402	64.2911
		0.0120			6.1596	0.9219	0.4561	75.31.5
15.00	0.150	0.0120	0.5000	C.0250	U.1435	0.4965	0.5308	80.5053
		0.0120			0.1969	1.0683	0.5757	66.5337
		0.0120			0.2101	1.1356	0.6137	90.5527
						•		
2 00	C 150	0.2120	0.7676	C C.750	0.0403	0.2546	0.1155	17.4029
		0.7123			U.1383	1.0523	0.4402	71.4573
		0.0120			0.1510	1.1530	0.4551	71.7.43
		0.7120			0.1632	1.2491	0.5308	83.1347
		0.0120			0.1032	1.3367	U.5757	69.3417
		0.0120						93.5591
22.00	0.150	0.0120	7. 1010	0.0290	0.1369	1.4232	0.6157	93.3391
		0.0120			0.0378	0.2673	0.1155	17.6544
		0.0120			0.1295	1.1950	0.4402	76.2733
		0.0120			0.1412	1.3133	0.4601	76.9000
		0.3120			0.1527	1.4217	0.5308	84.4730
		0.0120			U. 1537	1.5274	0.5757	9065174
22.00	C-150	0.0120	J. 86£L	(.0250	0.1744	1.0275	0.6167	95.1753
2.00	C.150	0.0120	0.9659	0.0250	0.0365	0.3073	0.1155	17.73+3
		0.0120			0.1249	1.2841	0.4402	73.1070
		0.0120			0.1364	1.4067	0.4861	74.5934
		0.0120			0.1473	1.5247	0.5308	85.1353
		0.3123			i.1576	1.5402	0.5757	71.5732
		0.0120			U.1623	1.744+	0.6107	95. 1001
2.00	0-150	0.0120	0.5562	0-(250	0.035 2	0.3123	0.1155	17. :15J
		0.7120				1.3090	0.4402	73.32.3
		0.0120			0.1237	1.4350	U-4801	75.7525
		0.7120				1.7545	U-530 #	62.3723
		0.3120			6.1954	1.0704	0.5302	91.7013
		0.0120			U.1554	1.7501	0.0107	96.1901
22000	(0 2) (00 /1.0	0.7-02	0.05.70	0.5.10(1.7501	0.0107	,0 .1 .0 1

		maan. Coefe	SUPPLY SLUPE (SIN)	SE/ DC	DRAIN FLOW ENTRY DEPTH PATIO NVD.		NURMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPTH LZO:
	,							:
00	0.150	0.0120	0.7586	0.6125	0.0550	0.1413	0.1449	10.07.1
		0.0129			0.1732	0.5574	0.570H	66.4713
		0.0120			0.21.5	0.5077	0.0323	76.7125
				(.0125)	6.2244	0-5544	3.5124	74.5020
		0.1120			L • 245	0.5760	9.7534	77. 139
20	(.150	0.0120	(- 2 : 5 0	0.0125	0.2634	0.7417	0.8120	00.4315
63	(.150	0.1133	0.5000	0.0129	0.0448	0.2071	0.1447	19.1021
0.0	0.150	0.0129	0.5000	C.(125	0.1552	0.0430	50700	71.3552
		C:0133			(.1595	0.9219	0.03.3	76.1.12
		0.0120			v.1535	0.7955	0.5764	20.3712
		(.)150			6.1369	1.0663	0.7554	24.3000
)3	0.150	C.)120	5.5(66	(.(125	0.2111	1.1356	0.5123	07.2193
03	0.150	0.7120	0.7070	0.0175	0.0403	0.4545	Ü. 1449	17.0925
		0.0120			0.13:3	1.0:23	0.570ā	77.3223
		0.2123			0.1510	1.1530	0.5323	50.3341
0.5	(.150	0.0125	0.7676	C.C125	0.1532	1.2491	0.6929	04.3124
00	6.150	C. 0139	7.7176	0.1725	0.1752	1.3357	0.7034	60.3504
00	(.150	0.0120	0.7676	C. U175	0.1009	1.4232	0.3120	90.7032
20	0.150	0.0120	0 8160	((3.95	0.0375	9.2673	0.1449	19.5950
		0.7120				1.4955	Ú.57UA	84.0302
		0.0120			0.1412	1.5133	0.6323	04.54.3
		0.0120			6.1547	1.4617	0.6929	50.3017
		6.0123			0.1037	1.5274	3.7534	67.2253
, L.O	(.1:(0.3123	n. Erct	(.0125	0.1744	1.6275	3.3120	102272
	(-150	0.3170	7.4,50	0.6125	0.5355	0.3373	0.1449	20.0315
				(.:175	0.1249	1.2541		67.5340
				(0.1304	1.4067		cu.41.5
		0.0125			U.1473	1.5647	0.6929	
. O J	0.150	0.0123	0.6659	0125	0.1075	1.5402	0.7534	27.6313
.00	0.150	0.0120	0.9654	C.(17%	3.1533	1.7447	0.5120	105.1937
. en	C . 14 C	C. 1121	0 064	(.(125	Ŭ•0352	0.5123	U.1449	20191
				0.0125		1.3070		
				C.(125	0.1344	1.4363		00.15.7
				(13%		1.0045		
				C. 0125		1.0704		
				(.0175		1.7561	0.5120	
								,

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2.0 14.1 16.6 14.0 20.0 22.0

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FLOW	DIA.	MANN.	SUPPLY	PEATN	DRAIN FLOH	ENTRY	NORMAL	PIPE LENGTH TO
L/S.	Pi-	CJEFF	_	SLOPE	ENTRY DEPTH		DEPTH	NORMAL DEPTH.
			(SIH)	(SIN)	RATIO H/L.	M.	H/D.	L/D.
-								
								*
								•
			0.077		4. 0. 70			17 70:
		0.0120			0.0550	0.1413	0.1320	17.7315
		0.0120			6.1932	0.0574	0.5112	67.7004
16.00	0.150	0.2120	0.2586	0.6167	U. 2115	0.6077	U.5659	73.2215
18.00	0.150	6.3120	9.2566	(.6167	0.2244	0.0544	0.6140	70.1400
20.00	0.150	0.0120	0.2568	6 - 61 67	0.2456	0.6460	0.6724	84.3035
_	_	0.0120			√°0 . 2634	0.7417	0.7241.	05.9427
22.00	0.100	0.7220	0.2.20	(•010:	.0.5024	0.1411	0.1211	0347721
		0.0120			0.0448	0.2071	0.1320	18.8156
14.00	0.150	0.0120	0.5000	0.0167	0.1552	0.8430	0.5112	72.5674
16.00	0.150	0.0120	0.5000	0.0167	0.1676	0.9219	0.5659	70.5709
		0.0130			0.1835	0.4465	0.6196	9702 د ه
		0.0120			0.1909	1.0683	0.6724	60.7131
							9.7241	92.7354
22.00	0.150	0.0120	0.5666	0.0157	0.2101	1.435t	9.7241	92.1354
2.00	C.15C	0.0120	0.7070	C.6167	0.0403	0.2546	0.1320	14.2565
14.00	0.150	0.0120	0.7676	0.0167	0.1383	1.0523	0.5112	74.73.3
		0.0120			0.1510	1.1530	0.5654	80.9703
				C. 6167	0.1632	1.2491	0.6146	80.6917
		0.0120			0.1752	1.3387	0.6724	91.5330
22.00	0-150	0.0120	0.7070	0.0157	0.1309	1.4232	0.7241	95.7534
2.00	0.150	0.0120	0.8660	0.6167	0.037d	0.2573	0.1320	19.5303
14.00	0.150	0.7120	0.8660	(.0147	0.1295	1.1958	0.5112	75.5725
16.00	C.150	0.0120	0.8660	C. C167	0.1412	1.3133	0.5659	84.2333
		0.0120			0.1527	1.4217	0.5176	80.9533
		0.0120			v.1537	1.5274	0.0724	91.7010
		0.0120			0.1744	1.0276	0.7241	29.1617
22.00	1.150	0. 1120	0.8666	0.0157	0.1/44	1.02/0	0.7241	29.1017
		0.0120			0.0355	0.3073	0.1320	19.6543
14.00	0.150	0.0120	0.9655	C. 0167	0.1249	1.2841	0.5112	77.2913
16.00	C.150	0.0120	0.5654	0.6157	0.1364	1.4067	0.5659	91.5040
13.00	0.150	6.0120	0.4659	Ca6167	0.1473	1.5247	0.6146	80.1949
		0.0120			U.1578	1.0402	0.6/24	91.2730
		6.0120			0.1603	1.7449	0.7241	90.5731
22.00	(. 1) (0.011.0	70 9039	6.0107	0.1003	7.1444	3.7241	70.5737
		0.0120			0.0362	0.3123	0.1329	19.6453
		0.0120			0.1237	1.3090	0.5112	77.7)
16.00	C.150	0.0120	0.5962	0.0167	0.1349	1.4300	J. 5659	93.7633
14.00	0.150	0.0120	0.5462	C.U157	0.1454	1.5545	0.6115	55.9773
		0.7123			0.1504	1.6704	J. 0724	91.10.3
		0.7120			0.1506	1.7801	0.7241	84.7704
2200	0.10	0. 11.0	00 / 762	COCTCL	0.1300	101001	0.1271	04.7704

FLOW L/S.	DIA.	HANN.	SUPPLY	DPAIN SLUPE	DRAIN FLOW ENTRY DEPTH	ENTRY	NORHAL DEPTH	PIPE LENGTH NORMAL DEPTH	
	Fi e	CUEFF	(SIN)	(SIN)	RATIO H/D.	H.	H/D.	L/D.	
							•.	•	
							7		
	*								
			0.2588		0.0633	0.1100	0.1068	8.6502	
			0.2588		0.2250	0.4236	0.4021	35.6544	
			0.2568		0.2468	0.4601	0.4436	36.8557	
			0.2566 0.2566		C.2678	0.4949	0.4841 0.5239	41.6134	
			0.2586		0.3053	0.5277	0.5630	44.5253 46.9423	
22000	0.130	0.7170	0.2700	0.0000	0.3033	0.7760	0.0000	70.7723	
									-
			0.5000		0.0515	0.1597	0.1068	9.6042	
			0.5000		0.1801	0.6357	0.4021	39.6793	
			0.5000		0.1969	0.6943	0.4436	43.3195	
			0.5000		0.2133	0.7492	0.4841	46.6002	1
			0.5000		0.2241	0.8015 0.3494	0.5239 0.5630	49.6710 52.3477	1
22.00	0.150	0.010	0.500	0.0500	0 . 2 77 9	0.5474	0.7630	32.571.7	7
					,				2
2.00	0.150	0.0150	0.7076	0.0500	0.0462	0.1953	0.1068	9.9902	
			0.7076		0.1603	0.7922	0.4021	41.3743	
			0.7070			0.8662	0.4436	45.1762	
			0.7070		0.1896	0.9361	0.4841	40.5256	1
			0.7070		0.2037	1.0008	0.5239	51.8248	1
22.00	0.150	0.0153	0.7070	0.0500	0.2174	1.0636	0.5630		1
									2
2.00	0.150	0.0150	0.8660	0.0500	0.0434	0.2201	0.1068	10.1803	in.
14.00	0.150	0.0150	0.8666	0.0500		0.9021	0.4021	44.2502	
			0.8660		0.1637	0.9864	0.4436	40.1423	
			0.8660		G.1771	1.0663	0.4541		1
			0.0666		0.1901	1.1433	0.5239		1
22.00	0.150	0.7150	0.8660	0.0500	0.2028	1.2157	0.5630		1
					15				21
2.00	0.150	0.0150	0.9659	C.0500	0.0420	0.2350	0.1068	10.2894	
			0.9659		0.1447	0.9647	0.4021	42.6860	
			0.9659		C. 1578	1.0552	0.4436	40.6325	2
			0.6659		0.1708	1.1441	0.4841		1
			0.9659		0.1932	1.2270	0.5239	No.	lé
22.00	0.150	0.0150	0.9659	0.0500	0.1954	1.3051	0.5630		1:
									20
2.00	0.150	0.2150	0.9962	C-0520	0.0415	0.2397	0.1068	10.3135	2
			0.9462		0.1432	0.4839	0.4021	42.5073	
			0.9962		0.1564	1.0775	0.4436		2
			0.9962		0.1691	1.1666	0.4541	50.3404	4
			0.9962		0.1813	1.2527	0.5239	53.7133	5
22.00	0.150	0.0150	0.9962	0.0500	0.1935	1.3307	0.5630	50.7227	8
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FLOW L/S.	BIA.	HANN. CJEFF	SUPPLY SUPPLY	DFAIN SLUPE (SIN)	DRAIN FLOH ENIRY DEPTH RATIO M/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH TO NORMAL JEPTH: L/D:
2 04	6 150	0.0150	0 3566	0.0350	0 0-22	0 1100	0 1227	10.7377
		0.0150			0.0533 U.2250	0.1100	0.1337 0.5200	41.1627
		0.0150	_		0.2468	0.4601	0.5757	44.3400
		0.0150			U.267a	0.4949	0.6294	40.5270
	_	0.0100			0.2363	0.5277	V-6511	49.0690
		0.7150			0.30±3	0.558	0.7368	51.5523
22.00	0.1.70	0.7270	502500	0.02,70	0.0000	0.000	0.7500	316 333 3
				•				
2.00	0-150	0.0150	0.5000	0-0250	0.0515	0.1597	0.1337	11.5501
		0.0150			0.1801	0.6357	0.5200	44.7311
		0.0150			0.1969	0.6943	0.5757	40.2533
		0.0150			0.2133	0.7492	0.0294	51.4270
		0.7150			0.2291	0.3015	U.6031	53.7000
		0.3150			0.2449	0.5494	U.73c8	50.451
					,			
2.00	0.150	0.0150	0.7070	C. C250	0.0402	0.1953	0.1337	11.9140
14.00	0.150	0.0150	0.7070	0.0250	0.1603	0.7922	0.5200	40.3445
16.00	0.150	0.0150	0.7076	0.0250	0.1752	0.8062	0.5757	50.0559
18.00	0.150	0.2150	9.7076	0.0250	0.1546	0.9361	0.6244	52.0577
20.00	0.150	0.0150	0.7070	C. C250	0.2737	1.0008	0.6831	55.7755
22.00	0.150	0.0150	0.7070	0.0250	0.2174	1.0635	0.7308	50.7010
		0.0150			0.0434	0.2201	0.1337	12.1030
		0.7150			U.1498	0.9021	0.5200	47.2074
		0.7151			0.1637	0.9364	0.5757	51.0013
		0.0150			0.1771	1.0663	0.6294	53.9005
		0.0150			0.1931	1.1433	0.6531	5029103
22.00	0.150	0.)150	0.8666	0.0250	0.202 s	1.2157	0.7368	59.9127
2.00	C 150	6 0150	0.0150	0.0353	0.04.4	0 3350	0.1253	3.5. 5.
		0.0150			0.0426	0.2350	0.1337	12.2006
		0.0150			0.1447	0.9647	0.5200	47.6294
		0.0150			0.1578	1.0532	0.5757	51.4557
		0.3150			0.1758	1.1441	9.62+4	54.4275
		0.7150			0.1832	1.2270	0.6831	57.4012
22.00	0.150	0.7170	9.9659	(.(250	U.1 154	1.3051	0.7308	66.5247
2.00	0-166	C. 2150	0 6642	r (250	0.0415	0.2397	0.1337	12.22/0
		0.7130			0.0415	0.4539	0.5200	47.7443
		0.0150			(.1504	1.0775	0.5757	51.5007
		0.0150			0.1571	1.1566	0.5757	54.5721
		0.0150		_	6.1313	1.2527	0.6431	57.0440
		0.3150			0.1735	٠٠ 307 -		60.357
	04170	0.000	00 7702	0.0270	0.1733	1.3301	7. 1300	00.000

					,	•	•	
FLOW E/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIN)	DRAIM SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORHAL DEPTH H/D.	PIPE, LENGTH NORMAL DEPT L/D.
							**	
	*							
2.00	0-150	0.9150	0.2588	0.0167	0.0633	0.1100	0.1527	11-0444
		0.0150			0.2250	0.4236	0.6000	30.0321
16.00	0.150	0.7150	3382.0	C.0167	0.2468	0.4501	0.6724	40.1312
		0.0150			0.2676	0.4949	0.7308	41.6353
_		0.0150			0.2803	0.5277	0.8013	42.8944
22.00	0.150	0.0150	0.2588	0.0167	0.3083	0.5588	0.8647	43.7873
				,			•	
2.00	0.150	0-0150	n - 5000	C.0167	0.0515	0.1597	0.1547	11.8447
		0.0150		•	0.1801	0.6357	0.6000	41.6011
		0.0150			0.1469	0.6943	0.6724	44.0872
		0.0150			0.2133	0.7492	0.7308	45.9453
		0.0150			0.2271	0.8015	0.8013	47.5525
22.00	0.150	0.0150	0.5000	0.0167	0.2449	0.5494	7 265 6	40.7473
					,	•		
2 60	0 150	6 2150	0 7070	0 07.47	6 04/3	0 1053	0.1517	12 2020
		0.0150			0.0462	0.1953 0.7922	0.1527	12.2030 43.2469
		0.7150			0.1603 0.1752	0.1922	0.6724	42.904
		0.0150			0.1396	0.9361	0.7368	47.9259
		0.0150			0.2037	1.0005	0.6013	44.6751
		0.3150			0.2174	1.0636	0.8047	51.0290
		0.0150			0.0434	0.2201	0.1527	12.3939
		0.0150			0.1498	0.9021	0.6050	44.4383
		0.0150			0.1637 0.1771	0.9864 1.0663	0.6724 0.7358	46.5291 49,3657
		C. 7150			0.1901	1.1433	0.8013	50.2755
		0.0150			0.2028	1.2157	0.8647	52.2072
							•	
		0.3150			0.0420	0.2350	0.1527	12.4929
		0.0150			0.1447	0.9647	0.6060	45.2875
		0.0150			0.1570	1.0562	0.6724	40.4157
		0.7150			0.1708	1.1441	0.7355 0.8013	50.1553 50.5714
		0.0150			0.1832 0.1954	1.2270	0.8547	52. 9023
22.00	0.150	0.0170	0.7657	0.0161	0.1777	1.3031	0.0347	72.0023
2.00	0.150	0.0150	0.9962	0.0167	0.0415	0.2397	0.1527	12.5213
14.00	0.150	0.3150	0.9962	0.0167	0.1432	0.9539	0.6060	45.5317
		0.7150				1.0775	0.6724	40. 7557
		0.7150				1.1066	0.7308	50.3703
		0.0150			0.1313	1.2527	0.6013	50.0567
22.00	0-120	0.7150	0.9562	0.0157	U-1935	1.3307	0.8547	52.9617

						•		
FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SL(PE (SIN)	DEAIN SLUPE (SIN)	DRAIN FLOH ENTRY DEPTH RATIO =/O.	ENTRY ENEPGY M.	NORMAL DEPTH H/D.	PIPE LENGTH TO NORMAL DEPTH: L/D:
								•
2.00	0-150	0.0150	0.7588	0-0125	0.0633	0.1100	0.1661	10.3002
		0.7150			0.2250	0.4236	0.6702	29.3771
		0.0150			0.2403	0.4601	J. 7534	24.123
18.00	0.150	0.0150	0.2580	0.0125	U.2078	0.4949	0.8207	24.7727
		0.7150			0.2303	0.5277	.0.8999	24.0130
22.00	0.150	0.0150	0.2586	0.0125	U.3033	0.5565	0.9722	29.0737
			٠,	,				
2 00	0 150	0.0150	D E C C (:	0.03.26	0.0515	0.1597	0.1681	11.1153
		0.0150			0.1301	0.6357	0.1001	32.2441
		0.0150			0.1969	0.6943	0.7534	34.53.6
		0.0150			0.2133	0.7492	0.8267	37.4175
		0.7150			6.2291	0.8015	0.8999	31.4574
		0.2150			0.2447	0.5494	0.9722	34.0007
		0.)150			0.0402	0.1953	0.1601	11.4823
		0.0150			0.1603	0.7922	3.6732	33.3577
		0.0150 C.0150			0.1752 0.1896	0.5662	0.7534 0.8267	30.2501 37.3354
		0.)159			0.2037	1.0003	J. 5999	31.3203
		0.7150			0.2174	1.0635	0.9722	32.6113
			••••					
		0.7150			0.0434	0.2201	0.1651	11.6752
		0.7150			U-1470	0.7021	0.67.2	33.3373
		0.7150			0.1637	0.9564	0.7534	37.1323
		0.0150 0.0150			0.1771	1.0063	0.6267	37.7.045
		0.0150			0.1901 0.2028	1.2157	0.8949	29.7345 36.4330
	0 6 2 7 0	0.011	00000	0.0127	0.2020	102171	V 17122	JU 6 1 J J U
2.00	0.150	0.0150	0.9659	0.6125	0.0420	0.2350	0.1651	11.0391
		0.7150			0.1447	0.9047	0.67.2	34.0201
		0.0150			U.1573	1.0582	0.7534	37.5000
		C. 3150			0.1708	1.1441	0.8207	30.0357
		0.0150			0.1:32	1.2270	0.8444	27. 5503
22.00	0.150	0.3150	0.9659	0.0125	0.1754	1.3051	0.4722	30.3254
2.00	C.150	0.3150	0.4562	0.(125	0.0415	0.2397	J. 1531	11.7053
		0.7150			0.1432	0.7039	0.6732	34.0043
15.00	0.150	6.7150	0.491.2	0.0125	U . 1564	1.0775	0.7534	37.6107
		0.1150			0.1071	1.1566	J. 0207	30.1110
		0.7150			0.1313	1.2527	0.59 19	20.7111
22.03	0.150	0.0150	0.5962	0.0125	0.1935	1.3307	J. 9722	30.9254

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLGPE (SIN)	DFAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY M.	NORMAL DEPTH H/D.	PIPE LENGTH NORMAL DEPTH L/D.
							·	
	•						•	:
2 00								
		0.0130			0.0710 0.2551	0.0906 0.3414	0.1201 0.4597	6.4455 25.7215
		6.0140			0.2530	0.3707	0.5063	20.05,7
		0.0130			0.3040	0.3957	0.5552	29.7735
		0.0130			Q•3279	0.4235	0.6021	31.7143
22.00	0.150	0.0130	0.2586	0.0500	ษิ.35∪8	0.4485	0-6479	33.3439
				•				
		0.0130			0.0577	0.1296	0.1201	7.1413
		0.0130			0.2035	0.5071	0-4547	26.6613
		0.0143			0.2223	0.5527	0.5083	31.2745
		0.7130			0.2416 0.2600	0.5952	0.5552	33.2354
		0.0130			0.2701	0.6719	0.6479	37.2013
2 00	0 150	0.0190	0 7070	0.05.00	0.0518	0.1579	0.1261	7. 4375
		0.0130			0.1810	0.1579	0.4597	29.94.2
		0.0130			0.1951	0.6863	0.5083	32.5757
		0.0130			0.2145	0.7413	0.5552	34.7741
		0.0130			0.2306	0.7920	0.6021	37.0753
22.00	0.156	0.0130	0.7070	0.0500	0.2463	0.5400	0.6479	39.0296
								. 2
2.00	0.150	0.0130	0.8660	0.0500	0.0456	0.1777	0.1201	7.5925
		0.0130				.0.7157	0.4597	30.6337
		0.3139			0.1349	0.7513	0.5053	33.4233
		0.0130			0.2003 0.2152	0.8430 0.9018	0.5552 0.6021	35.5307 37.5433
		0.7130			0.2296	0.9537	0.6479	39.9742
								11
2 - 0.0	0.156	0.0110	0.6456	C. 0500	0.0470	0.1596	0.1201	7.6719
		0.0130			0.1632	0.7653	0.4597	30.9615
		0.0130			0.1763	0.8371	0.50±3	33 - 8020
		0.0130			0.1930	0.9047	0.5552	30.0002
		0.0130			0.2074	0.9674	0.6021	36.3945
22.00	0-150	0.7130	0.9659	0.0500	0.2213	1.0281	0.6479	40.4455
								20
		0.0130				0.1929	0.1201	7.0424
		0.0130			0.1615	0.7803	0.4547	31.0074
		0.0130			0.1764 0.1910	0.4548	0.5003 0.5552	33.9157
		0.7130			0.1910	0.9224	0.6021	30.5147
		0.0133			0.2109	1.0500	0.6479	40. 2545
								1116

FLOW L/S.	CIA.	MANN.	SUPPLY	DPAIN SLUPE	DRAIN FLOW ENTRY DEPTH	ENTRY	NORMAL DEPTH	PIPE LENGTH TO NORMAL DEPTH.
			(SEN)	(214)	RATIO H/G.	n.	H/D.	L/D.
•					,		•	
							•	:
	_							
2.00	0.250	0.0130	0.2586	C.0250	0.0710	0.0906	0.1508	7.3353
14.00	0-450	0.0130	0.2580	0.0250	0.2551	0.3414	0.5972	25.3315
		0.7130			0.2300	0.3707	0.6616	20.6107
		0.0130			0.3040	0.3987	0.7201	27.5004
		0.0140			0.3279	0.4235	0.7036	20.5459
22.00	0.150	0.0130	0.2588	0.0250	16.3508	0.4485	0.8511 .	29.1343
				•				
2.00	0.150	0.0130	0.5000	C.0250	0.0577	0.1296	U.15U8	7.9485
14.00	0.150	0.0140	0.5000	C.C250	0.2035	0.5071	0.5972	26.0321
		0.0150			0.2228	0.5527	0.6616	24.5923
		C.7130			0.2416	0.5452	0.7201	31.0134
		0.0130			U-2500	0.0347	0.7806	32.0136
22.00	0.150	0.0130	0.5000	C.(.250	0.2781	0.6719	0.8511	32.5590
					,			
2.00	0.150	0.7130	0.7070	0.0250	0.051b	0.1579	0.1508	8.2235
		0.0130			0.1810	0.6293	0.5972	29.2900
		0.0130			0.1951	0.0563	0.6016	36.9739
		0.0130			0.2145	0.7413	0.7201	32.5272
		0.9130			6.2306	0.7920	0.7806	33.64.7
22.00	0.150	0.0130	0.7070	0.0250	0.2463	0.0400	0.8511	34.6175
2 00	0 150	C. 0130	0 6640	0 6250	0.0486	0.1777	0.1508	0.3759
		0.0130			0.1691	0.7157	0.5972	29.9754
		0.0130			0.1849	0.7813	0.6616	31.7315
		0.0130			0.2003	0.0430	0.7201	33.34)7
		0.0130			0.2152	0.9015	0.7586	34.5319
22.00	0.150	0.0130	0.8660	0.0250	U.2296	0.9587	0. 5511	35.5759
2 00	0.150	0.0130	0.0454	0 6250	6. 0470	0 1907	0.15(0	5 65.3
		0.0130			0.0470 0.1632	0.1896-	0.1508 0.5972	6.4503 30.3143
		0.0130			0.1032	0.7633	0.5512	32.1145
		0.0150				0.9047	0.7261	33.7507
		0.0130				0.9674	J. 7806	34.955
		0.3130				1.0281	U. 8511	36.0557
H								
		0.0130				0.1929	0.1503	6.4770
		0.7130			0.1615	0.7508	0.5972	36.4136
		0.0130				0.0548	0.6616 U.7201	32.22.5 33.3007
		C-0133			0.1910	0.7224	J. 7886	35.1151
		0.3130			0.2169	1.0500	0.8511	30.2014
				,,,,	77227		340722	

FLOW L/S.	DIA.	MANN. COEFF	SUPPLY SLOPE (SIM)	DPAIN SLOPE (SIN)	DRAIN FLOW ENTRY DEPTH RATIO H/D.	ENTRY ENERGY H.	NORMAL DEPTH H/D.	PIPE LEAGTH T NORMAL DEPTH. L/O.
							,, 3	1
		0.0130			0.0710	0.0906	0.1725	6.5632
		0.0130			0.2551 0.2830	0.3414	0.6978	15.1757
		0.0130			0.3040	0.3707	0.8521	16.7734
	_	C. 71 10	_		0.3279	0.4238	0.9272	14.2745
		0.0130			0.3508	0.4485	1.0000	15.33.7
		0.0130			0.0577	0.1296	0.1725	7.1756
		0.0130			0.2035	0.5071	0.6978	22.3479
		0.0130			0.2228	0.5527 0.5952	0.7759 0.8521	18.7341
		0.0130			0.2416 0.2600	0.5952	0.9272	10.1867
		0.0130				0.6719	1.0000	17.4717
2.00	0.15C	0.0130	0.7070	0.0167	0.0518	0.1579	0.1725	7.4623
		0.0130			0.1910	0.6293	0.6978	21.7122
		0.0130			0.1901	0.0863	0.7759	19.3127
		0.7133			0.2145	0.7413	0.8521	20.8373
		0.7130			0.2306 0.2463	0.7920 0.8400	0.9272	25.0833 17.9951
22.00	0.150	0.3130	0.7676	0.0107	0.2463	0.0400	1.0000	11.7771
2.00	C-15C	0.0130	0.8660	0.0167	0.0406	0.1777	0.1725	7.6178
		0.7130			0.1691	0.7157	0.6978	21.9579
		0.0130			0.1349	0.7613	0.7759	19.3695
		0.1130			0.2003	0.5430	0.8521	21.5153
		0.0130			0.2152 0.2296	0.4018	0.9272	22.5173
22.00	0.170	0.1150	0.000	6.6101		0.7501	1.0000	2.007
2.00	0.150	0.0130	0.9659	C.0167	0.0470	0.1896	0.1725	7.6935
14.00	0.150	0.0130	0.9659	C.6167	0.1632	0.7653	0.6978	22.1253
		0.0130		-	0.1753	0.0371	0.7759	19.2514
		0.0130			6.1930	0.9047	0.8521	22.1145
		0.0130			U.2074 U.2213	0.9674	0.9272 1.00J0	22.27J7 17.5954
22300		00.170	0 6 70 5 7	()	V . L L I J	10000	20000	
2.00	0.150	0.0130	0.9962	C.0167	. 0 • 0465	0.1929	0.1725	7.7194
		0.0130			G.1615	0.7808	0.6978	22.1755
		C.0130	_		0.1764	0.8548	0.7759	14.1852
		0.3134			0.1910	0.9224	0.9521	22.1935
		0.0130	_		C.2052 U.2189	0.9872 1.0500	0.9272 1.00J0	22.2100 17.45)7
22.00	0.120	0.0120	0. 7762	C. 0101	0.4107	1.0300	7.0010	2101271

APPENDIX 2 DESCRIPTION OF PROGRAM PROFIL 2

Program PROFIL 2

This appendix presents a complete print out of this program together with sample input data. The program was run on the NBS CBT Perkin Elmer 732 computer.

The program accepts data in SI units with the exception of flow rate which is read in liters/second and corrected to m³/s within the program.

The program is effectively the first section of the hydraulic jump prediction program fully described in reference [1]. For this reason no detailed flow chart is included in this report.

	222222 2222222 22 222 22 22 22 22	66444666 66444666 66444666 6466666 6466666 6466666 6466666 6466666 6466666	01 01 00 00 00 00 00 00 00 00 00 00 00 0
7777277 7777777 777 777 777 777 777 777	313333 323 3333 3333 3333 33 33 33 33 33 3	* * * * * * * * * * * * * * * * * * *	48804 8488868 84 188804 188804 44 44 44 44 44 44 44 44 44 44 44 44 4
הורוור ונורוור וו וו וו וו וו וו	00 00000 00 000 000 000 000 000 000 00	10 10 10 10 10 10 10 10 10 10 10 10 10 1	
	00 00 00 00 00 00 00 00 00 00 00 00 00	71111111 711111111 711 711 711 711 711	######################################
	00000000000000000000000000000000000000	1.555557 5555555 5555555 555555 555555 555555	1 (10 P No 2017 2) (20 E O STAN 1 P NO E O STAN 1 P NO E O O O O O O O O O O O O O O O O O
00 00 00 00 00 00 00 00 00 00 00 00 00		00 00 00 00 00 00 00 00 00 00 00 00 00	
	33 33 33 33 33 33 33 33 33 33 33 33 33		0.000000000000000000000000000000000000
	0 % 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		

```
HOTALE
       PROGRAM PROFILE CALCULATES THE WATER SURFACE PROFILE
C
       IN SUPERCRITICAL FLOW FROM AN ENTRY CONCITION
C
       REPRESENTING TERMINAL CONDITIONS IN A STEEP SUPPLY PIPE
       TO THE ESTABLISHMENT UP THE NUPPAL DEPTH. IT IS TO be
       NOTED THAT THIS TRANSITION DUES NOT APQUIRE A HYDRAULIC
       JUMP AS THE FLOW IS SUPERCHITICAL AT ITS FULLY
C
       DEVELOPED CEPTH.
      JIMENSION > (2.100).F(2.100).IE(6)
      JIMENSION 5(2), EN(2,100), UEF (2,100)
      INTEGER SHAPE
      COMMON/CMI/E, C, G, C IN, SO, GAF, FFT:, FLR IT, MNURM, AREA, PER, FPM, ENERG
      COMMON/CH2/SHAPE >
      CUMMON/CH3/IZ
      READ(4.702)SHAPE
792
      FURMAT(I3)
      READ(4.12U) NE. NS. ICON
      READ(4,121)P, P, DEN
121
      FUKMAT (3F10.4)
      5=9.91
      IRUN=0
300
      IF ( | Z . G T . 1 ) | IF ( | Z ) = | S
      12=12+1
      IF(IZ.GT.2)1Z=1
      READ(4,100)PL, SC,G, HC)NT, ENZ
       5(12)=50
      IF ICON=1 THE FLOW ANALYSIS IS FASCO UN AN IMPUT ENERGY AT
      ENTRY TO THE MILD SLIPE PIPE, TERM ENZ. SIMILARLY THE LOSS
      COEFFICIENT AT PIPE ENTRY MAY UF EXPRESSED AS A FACTOR, JEN,
      VALUE O TO 1.6, TO BE MULTIPLIED BY THE ENZ TERM.
      AS THE ENTRY FLOW DEPTH IS TO BE CALCULATED FROM ENZADEN
C
      AND NOT BASEL ON FLOW CRITICAL LEPTH, THE CONTROL TERM
C
      HOONT IS SET TO 1.J. THE OTHER PARAMETERS REFER TO PIPE FLOW
C
      RATE AND DIFENSIONS.
100
      FURMAT(SFLC.4)
      IF (PL.EG. U.C)GCTU 3)1
C
      PL-PIPE LENGTH B-4107H. RM-MANNING CUEFF, SO-SLUPE.
C
      J-FLOWRATE IN L/S TO BE USED IN PREBAYS, HEUNT-CONTROL DEPTH
C
      SET TO ZERG IF CRITICAL DEPTH ASSUMED.
      J= 9/1000.U
      3-1000.0
      CUN=SM++2/SC
      JAM = G + RHG
C
      PRUGRAM CONTPUL DATA.
120
      FIRMAT(314)
C
      44-SIZE OF THE DH STEP IN SIMPSONS RULE INS-NU.
C
      STEPS IN CEPTH CALC., ICON CETEFFINES AHETMER ENERGY
      INPUT OR UPSTREAM SLOPE IS USED. DEN IS THE ENERGY
      LUSS FACTUR FOR THE PIPE ENTRY, IN EITHER ENTRY CASE.
      ENZ-INPUT ENERGY 10 REPLACE SLUPE IF ICON = 1.
      IF (ICON.EQ.1) GOTO 650
      JJ10 651
650
      ENZ=DEN#ENZ
      CALL BOUND (ENZ, C, B, H3)
      17=2
      3010 18
651
      CUNTINUE
      IF (HCUNT.EG.1.0) GDT9 17
                                                                        94
      SUTP 1 4
```

17

SHSD=GIN+LPGD

SALL REUND(FROD, C. 1. HI)

```
4CONT=HB "
18
      CUNTINUE .
      DETERMINATION OF CRITICAL AND NORMAL DEPTHS.
      THIS SECTION CALCULATES THE NORMAL AND CRITICAL DEPTH IN
      EACH PIPE LENGTH FOR LATER COMPARISON TO THE CONTROL SEPTH
      I.IPUT.
      CALCULATION OF CRITICAL DEPTH.
      JP = B
      JN=0.0
      1C=UP/2.0
      SUNTINUE
7
      CALL CALCIFCOLL)
      IF (HCRIT)J,4,5
3
      DH=HC
      3 DIGS
j
      JP=HC
      42N=(UP+DN) /2.0
6
      IF (A3S ( (HCN-HC)/HC) . LE . 0.001) GOTO R
      SUTH 7
      1C = HCN
3
      IF (HCGNT.EC.(.C)HC) YT=HC
C
      CALCULATION OF NORTAL DEPTH.
      14=8
      )N=0.0
      1N=UP/2.0
9
      SUNTINUE
      CALL CALC(H. P.EL)
      IF (HN394) 10,11,12
10
      HH=K(
      30TO 13
12
      15=HN
13
      14N=(UP+ON)/2.6
      17 (435 ((HNN-HN )/HN) .L. .D. .J. 1) 6676 14
      44=HNN
      SUTO 4
14
      AN=HNN
11
      CUNTINUE
C
      THIS SECTION PREPARES FOR THE PROFILE CALCULATIONS
C
      ST SORTING FLOWS BASED ON FIFE SLOPE AND THE MURNAL AND
C
      CRITICAL DEPTH VALUES.
      IF (HN.LT.HC) GOTO 50
C
      AILD SLOPE.
      IF (HCUNT.LT.HC) GGT9 45
C
      SUBCRITICAL FLOW, HODAT GT. HL.
      SIGN=-1.C
      JH= (HCGNT-HN)/FLUAT(NH)
      SUTO 60
C
      SUPERCRITICAL FLOW, HOOMT LT. HC.
45
      51GN=1.0
      JH=(HC-HCUNT)/FLOAT(NY)
      SUTO 60
      STEEP SLOPE, HN LT MC.
C
50
      IF (HCUNT.LE.HC) GGT7 55
      SUBCRITICAL FLOW, ACONT GI HC.
      51GH=-1.0
      JH= (HCUNT-HC)/FLOAT (MA)
C
      2010 50
C
      SUPERCRITICAL FLEW, HOCHT LT HC.
55
      31GN=1.0
      42=NN+2
```

JH= (HH-HCUFT)/FLCAT(H2)

95

```
60
      iL=0.0
      15=1
       IF (IZ.EQ. 1) GETC 947
      1=HCONT
      CALCIF, PL)
      E=ENEPS
      F.1=FPH
      IF ( I Z. GT. 1 ) F ( I Z-1, I S ) = F M
      IF(IZ.EQ.2)X(1,15)=).)
      IF(IZ.GT.1) DEP(IZ-1,15) =H
      if (17. GT.1) EN (12-1. [5] = [
       IF([2.FG.2] (UTO 313
C
C
C
                                   3
C
347
       CONTINUE
C
       THE APPRUACE PIPE LENGTH MAY BE IGNORED IF TERMINAL CONDITIONS
C
       ARE ASSUMEE. THIS SECTION USES THIS UPTICH BY CHECKING THE
C
       PIPE NUMBER . 12 . AND THE VALUE IF ICON WHICH IS SET TO 2.
       H=HN
       CALL CALC(F, LL)
       ENGO= ENENG
      TENT = HN
      EENT=ENGD
       JOTA 300
313
       CONTINUE
      HATER SUPERCE PROFILE CALCULATIONS USING SIMPSONS PULL
Ċ
      TO EVALUATE THE INTEGRAL.
      JJ 90 I=1, NS, 2
      5L0=5L
      15=15+1
      H2=HCCNT+SICF + UF +FL 3AT([+1]
       +3=HCGNT+SICN+FLCAT(I)+DH
      CALL CALCIFIELD
      SALL CALCIFE, LLZ)
      CALL CALC(F3, LL3)
      04=0H+(CL+(L2+4.C+)L3)/3.6
      SL=SL+DX
       1=H2
      CALL CALCIFICE)
      E=ENEKG
      5.4=FPM
       X(1,15)=5L
       JEP (1. IS) = H
       IF(H.SE.U.975*E) 3013 999
       IF(H.GE.U.975 $HN) 30TA 949
30
       SURITROS
999
       CONTINUE
       xFIN=x(1,IS)
       HFIN=HN
       G=0 $1000.0
       HENT= HENT/P
       HFIN=HFIN/B
       IF (HFIN.GT.C. 999) HFIN=1.C
       AFIN=X(1,15-1)+(C.975+MN-CEF(1,15-1))+(X(1,15)-X(1,15-1))/
     1 (DEP(1, [S) - CEP(1, [S-1])
       KFIN=XFIN/P
       IRUN= (FUN+1
                                                                          96
       TECTPUNGER .. I) WEITE(3,7)01
```

[F(Q.i U.Z.C)nFITE(3,7)9)

```
709
       FURHATI/16-X2
      write(3,701)0,8,RM,S(1),S(2),HENT,EENT,HFIN,XFIH
701
       FORMAT(1CX+F6.2+F6.3+3F7.4+3F10.4+F12.4)
       FORMATCIHI, ////. 10x. FLUW ", " CIA. ", " MANN.
700
       . SUPPLY . . LAZIN . . .
                                DRAIN FLEH ..
                                                LNTKY
                  .. PIPE LENGTH TU. . / .
     2.
        NORMAL
     310x, L/S. ","
                       P. ". CUEFF ". SLOPE ". SLUPE ".
                       ENERGY
                                 DEPTH
        . ENTRY DEPTH
                                           MCRHAL LEPTH. ..
    - 4 / . 29X . * (SIN)
                        (SIN) .
        PATIO H/E.
                                              -/0.4.//)
                        n.
                                  1:1C.
       IF (IRUN. EC. 36) IKUN=J
       GOTO 300
901
       CUNTINUE
       END
      SUBROUTINE BOUND (E. 7.3. HB)
      INTEGER SHIPE
      CJAHUN/CH2/SHAPE
      SUBPOUTINE EGUND CALCULATES THE ENTRY CONDITION TO THE
C
00000
      AILD SLOPE FIPE (IZ=2) BY REFLEENCE TO THE ENERGY AT
      DISCHARGE FFOR THE STEEP SLOPE PIPE (12=1), OR SIMPLY
      FROM THE EMEPEY INPUT DATA IF THAT MODE IS CHOOSEN
      THE LIPET OF ICON = 1 IN THE INITIAL READ STATEMENTS.
      PIPE CROSS SECTION IS CONTROLLED BY THE VALUE OF
      TERM SHAPE, 1=KECTANGJEAR OR Z=CIRCULAR, IN THE INPUT.
      3=9.81
      IF (SHAPE . ST. 1) GET 2
      11=0.0
      HB=C/(B+(2.0+6+E)++3.5)
      )H=H8/20%.C
      0.5/98=XF
      )U 75 I=1,160
      17(1.61.1) Y1=Y
       14 = 1 - X + D14
      1=(0++2)/(2.64G)+((3+14)++2)+(HX-E)
      IF(1.E0.1) (CTG 75
      IF(Y1.GF.O.O.AND.Y.LE.O.O) GETE 76
      IF(Y1.LE.G.C.AND.Y.GE.D.O) GOTO 76
75
      CONTINUE
76
      XH=UL
      SUTO 1
2
      BURITALS
       4=0.0
      EC1=0.0
       ) £ LH= £ /200 . 0
      21=3.142
      X=8/2.0
3
       H=H+DELH
       IF (H.LT.R) THE TA=2.0=ATAN(SQRT(H+(B-H))/(H-H))
       IF (H. EQ.R) THETA=PI
       IF(H-GT-R) THE TA=PI+2. G*ATAN((H-F)/(SGRT(H*(\theta-H))))
       AREA=((B**2)/6.C)*(THETA-SIN(THETA))
       EC2=H+(Q++2)/((AFEA++2)+2.0+C)
       IF(EC2.LE.E.AND.EC1.73.E) COTG 4
       EC1=EC2
       SUTO 3
       H = 6H
       CUNTINUE
       RETURN
       SND
       SUBROUTINE CALCIMATED
C
       SUBROUTINE CALC IS USED THRAUGHILT THE PROGRAM TO
```

DETERMINE THE FLUM-PIPE PARAPETERS SUCH AS FLUM

97

```
IN THE BISECTION METHOD CALCULATION OF NORMAL AND
C
      CRITICAL DEPTHS IN EACH OF THE PIPE LENGTHS. --
C
      IN THE CIRCULAR PIPE GROSS SECTION CASE IT ALSO
C
      CALCULATES SUBTENDED ANGLE AND THE WATER SURFACE .
C
      MINTH AS DEPTH CHAMSES.
C
      AS IN BOUND AND MAIN PROGRAM THE PIPE SMAPE IS DETERMINED
C
      BY THE VALUE OF THE TERM SHAPE INPUT AS CATA.
      INTEGER SHAPE
      COMMON/CHI/F.G.G.COM.SO.GAM.FHO.HCRIT.HNORM.AREA.FER.FPM.ENERG
      COMMON/CH2/SEAPE
      SIVEND/ NOMPOS
      IF(SHAPE-UT-1)GCTO 1
      IF([Z.EQ. J.ANE.H.GE.3]H=8
      AREA=H+B
      PER=8+2.0*F
      1CRIT=1.0-(C¢+2)+B/(G+ARFA++3)
      HADRH=1.0-(C**2)*CDM/((AREA**3.333)/(PER**1.333))
      JL=HCRIT/(HNCF#450)
      FPH= (SA##AREA#H/2.0)+(RHO#C#C/AFEA)
      EMERG=H+(U++2)/((AREA++2)+2.6+G)
      SUTO 2
1
      1=3 +C.5
      PI=3.142
      IF (IZ.EQ.3.AND.H.GE.A) GOTL 26
      IF(H.LT.R) THETA=2.000ATAN(SCRT(H0(3-H1))/(6/2.0-H))
      IF (H.EG.K) THETA=PI
      IF ( -- GT.R ) THE TA=P1 +2. J=ATAN((H-1/2.0)/(SuxT(++(b-4))))
      SS OTES
5.5
      4=3
      THETA=2.0 FF I
      AREA=P1+(E/2.0)++2
      PER=PI +9
      (0=5/2.0
      3310 21
22
      CONTINUE
      AREA=((BA42)/6.0)+(THETA-SIN(THETA))
      PER=9+THETA/2.U
      T=2.0+((H+(E-H))++).5)
      HCRIT=1.0-(C##2.0)#T/(G#AREA##3)
      HNORM=1.0-(C++2.0)+Clm/((AREA++3.333)/(PEK++1.333))
      DL=HCKIT/(HNCKH+SO)
      <0=(2.0/3.C)*(b/2.0)*(3.0*SIN(THETA/2.))-SIN(3.0*THETA/2.0))</pre>
     1/(4.0=(THETA/2.0-0.5=SIN(THETA)))
      104 R= X 0+H-t/2.0
21
      FPM=GAM+AREA+HEAR+RHC+U+C/AREA
      ENERG=H+(G++2)/((AREA++2)+2.C+G)
2
      CONTINUE
      RETURN
      GMB
CF361
```

Sample data program PROFIL 2.

- Line 1. SHAPE, Format I3.

 Geometry indicator 2 = circular pipe $\nabla\nabla$ 2
- Line 2. NN, NS, ICON, Format 314

 NN dh interval on depth profile

 NS N° calculation steps, max., Simposn Rule

 ICON 2 assumes terminal conditions in approach pipe

 VV30 V200 VVV2
- Line 3. B, RM, DEN, Format 3F10.4
 B pipe diameter, RM Manning Coeff.,
 DEN entry energy loss coefficient
 VVVV0.1500 VVVV0.0090 VVVV1.0000
- Line 4. PL, SO, Q, HCONT, ECZ, Format 5F10.4
 PL pipe length, SO pipe slope, Q flow rate
 HCONT control depth indicator, O value
 indicates upstream critical control,
 ENZ entry energy, zero unless ICON = 1.
 VVVV40.0000 VVVV0.0070 VVVV4.0000 VVVV0.0000 VVVV0.0000

Note, line 4 is approach pipe data.

- Line 5. PL, SO, Q, HCONT, ENZ, Format 5F10.4

 HCONT = 1 indicates entry depth as control

 Line 5 is test pipe data

 VVVV40.0000 VVVV0.0250 VVVV4.0000 VVVV1.0000 VVVV0.0000
- Line 6, 7; 8, 9; etc repeat format 4, 5; for all test cases
- Last line. PL, SQ, Q, HCONT, ENZ, Format 5F10.4 zero values terminate run. VVVV0.0000 VVVV0.0000 VVVV0.0000 VVVV0.0000

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The criteria governing the development	of steady partially fill	ed supercritical				
pipe flow are presented together with t	he necessary techniques	to determine the				
water surface profile in the pipe entry	transition length.					
The establishment of full bore flow is						
pipe design parameters. Based on the w	-	-				
pipe length predictions are presented t		fluctuations in the				
drainage system that result from full bore flow establishment.						
Tabular data is presented to allow design decisions to be made that link pipe						
slope, diameter and roughness to the need to avoid full bore flow. A graphical						
technique is also presented that removes the necessity to interpolate from the						
tabular data.						
The effect of entry geometry loss coefficients is included in the techniques presented.						
presented.						
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